



Upper Barataria Basin, Louisiana Feasibility Report

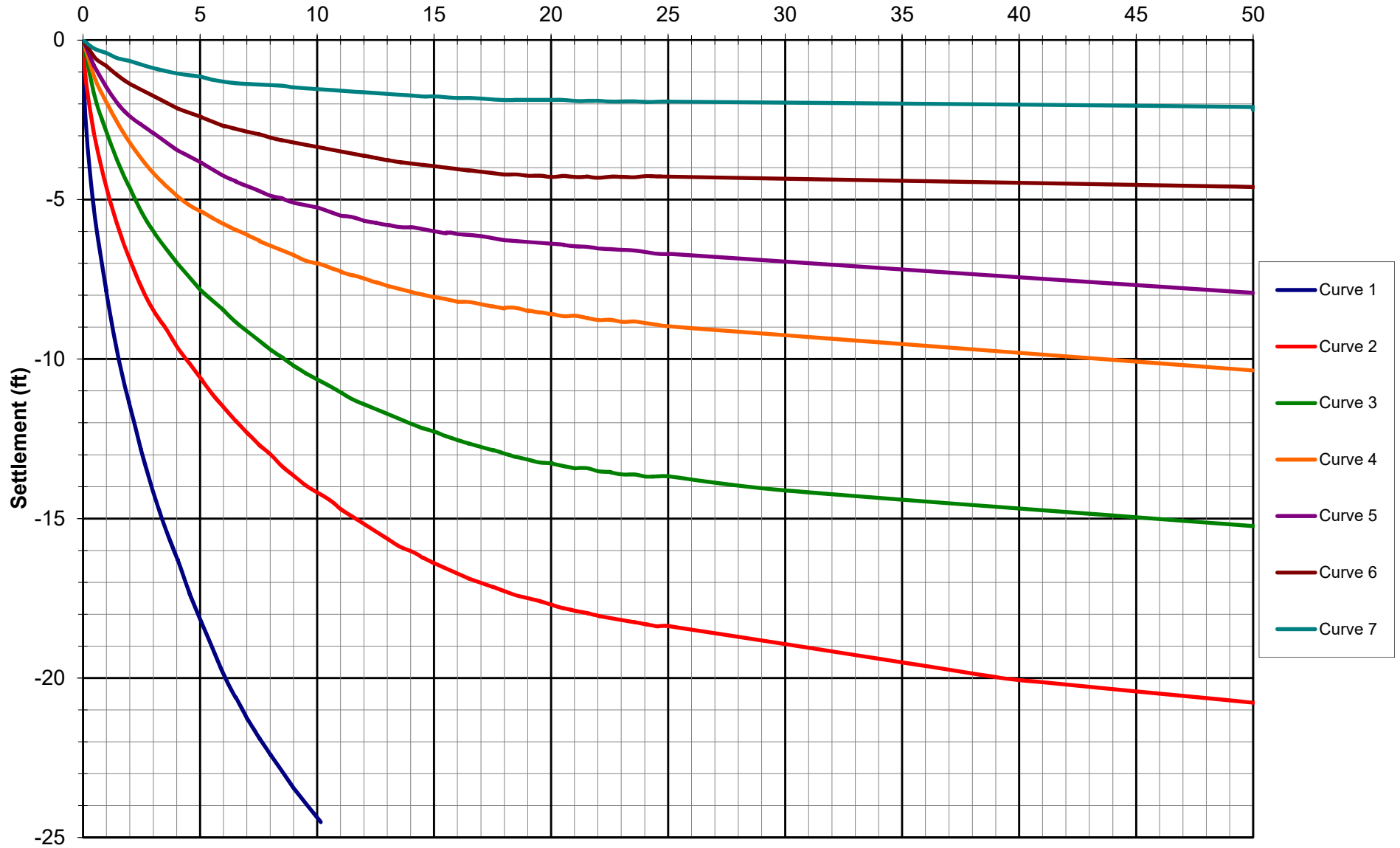


Appendix A: Annex 2 – Final Screening Phase: Geotechnical Drawings

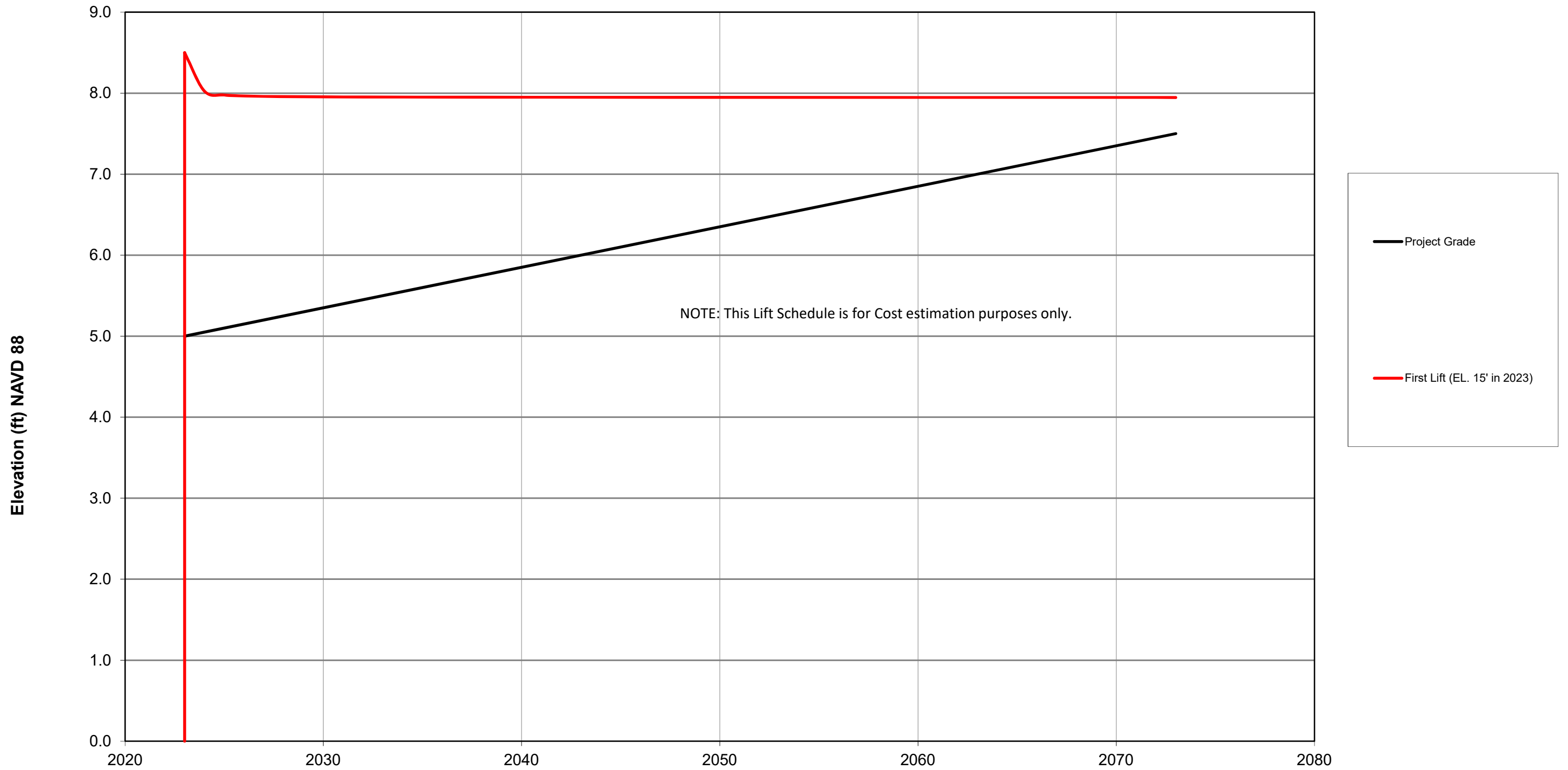
December 2021

Upper Barataria Basin, LA - Feasibility Study Settlement - USACE Family of Curves

Time (yrs)



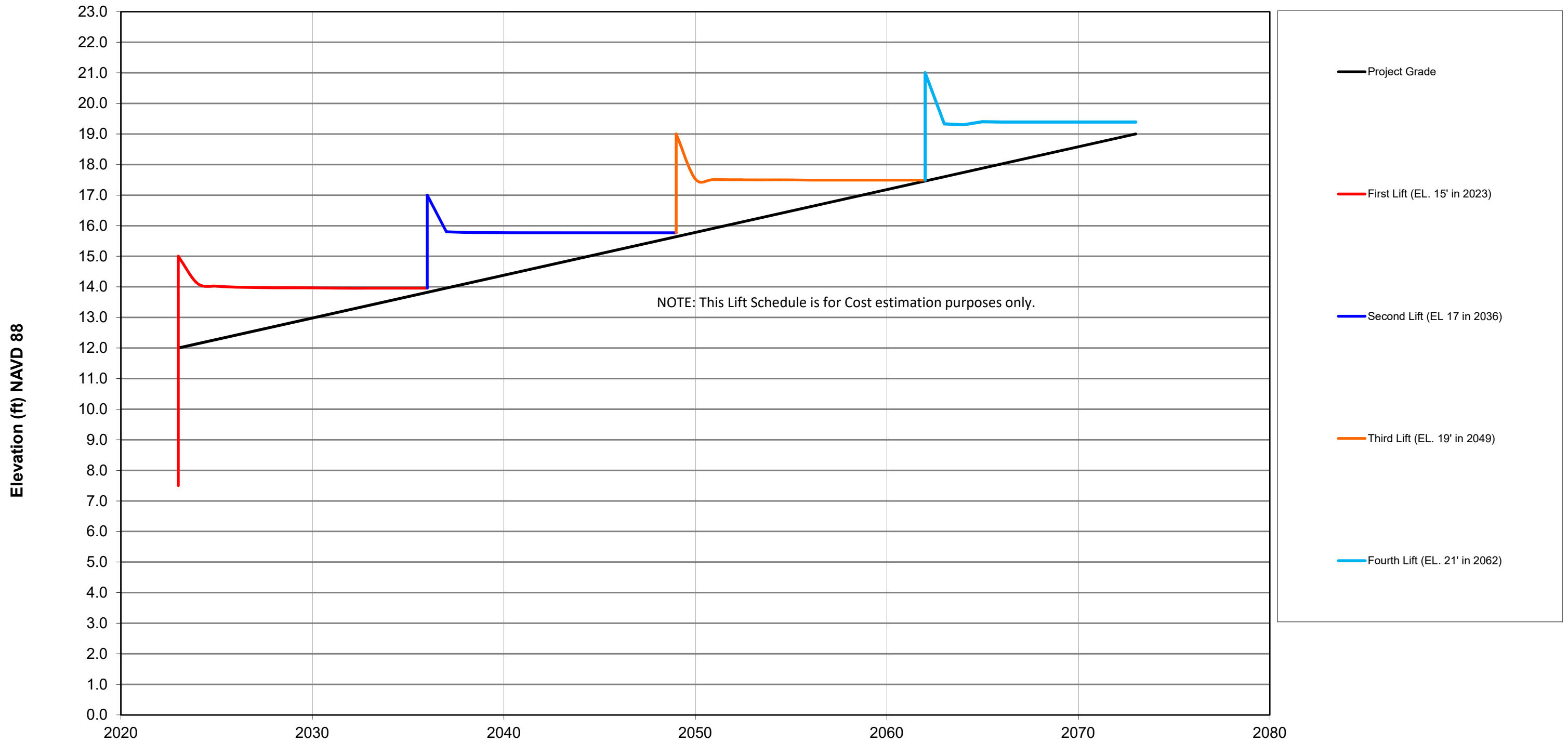
Upper Barataria Basin Lift Schedule for Alternatives 1, 3 , and 5



NOTE: This Lift Schedule is for Cost estimation purposes only.

Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.

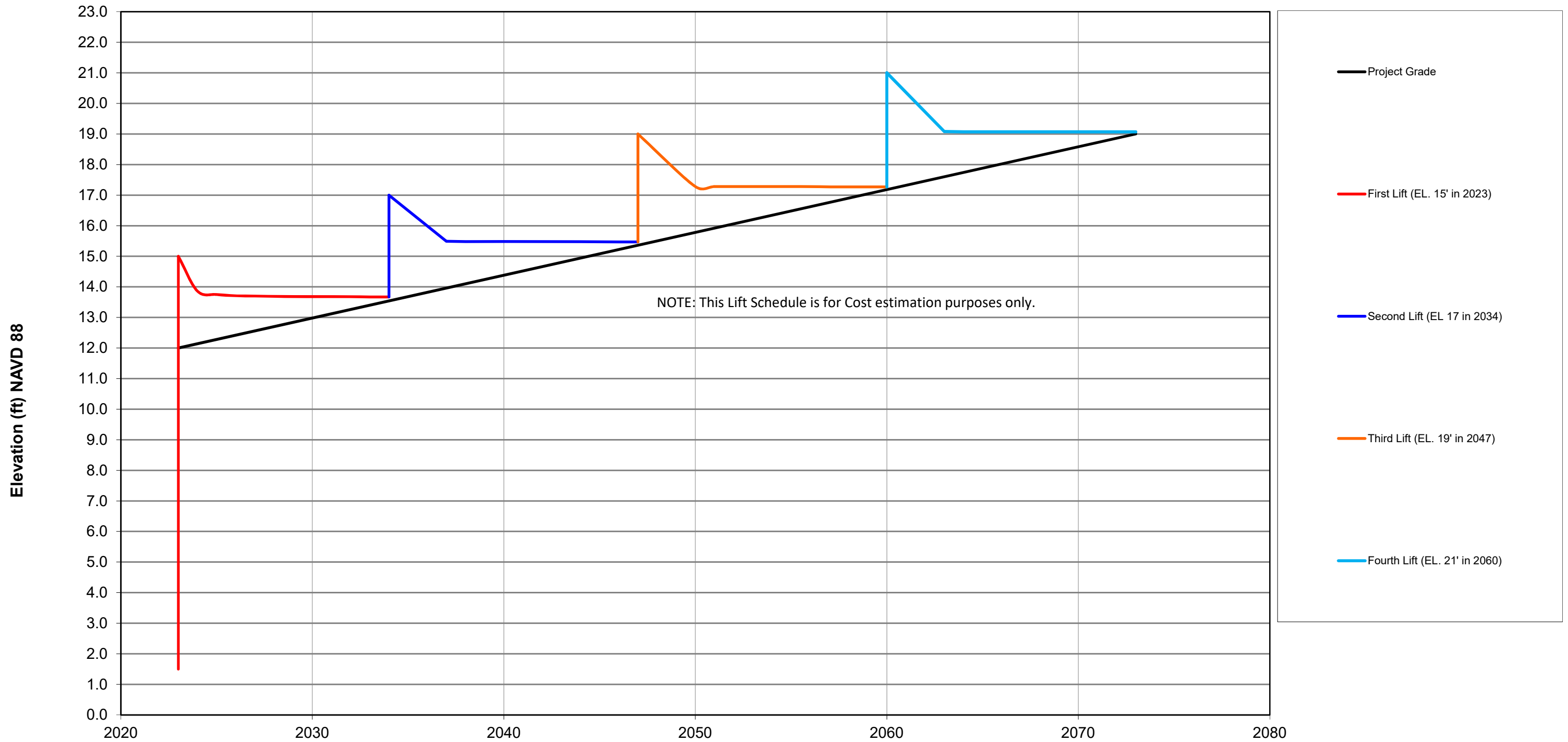
Upper Barataria Basin Lift Schedule - Alternative 6 Reaches A, B and C



NOTE: This Lift Schedule is for Cost estimation purposes only.

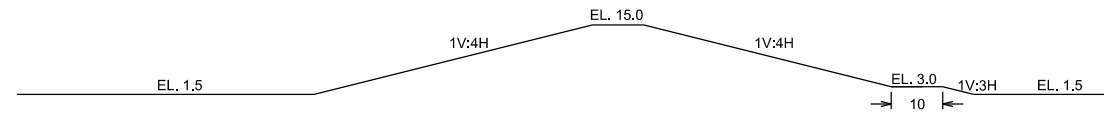
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.

Upper Barataria Basin Lift Schedule - Alternative 6 - Reaches D, E, F, G, H and K

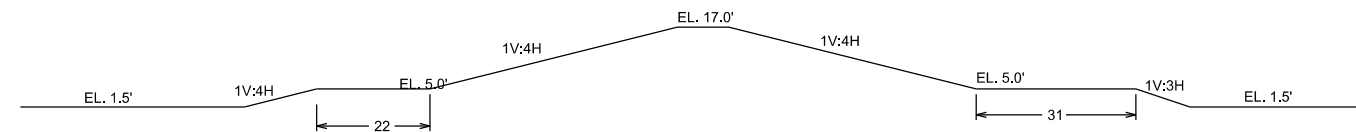


NOTE: This Lift Schedule is for Cost estimation purposes only.

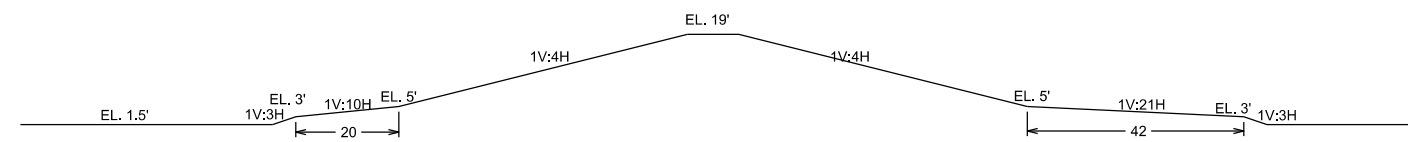
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.



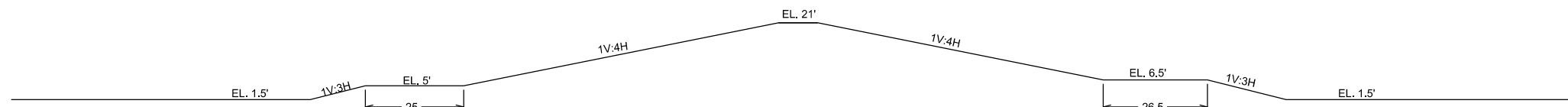
EL. 15' Upper Barataria Basin Section for Cost Estimation Purposes



EL. 17' Upper Barataria Basin Section for Cost Estimation Purposes



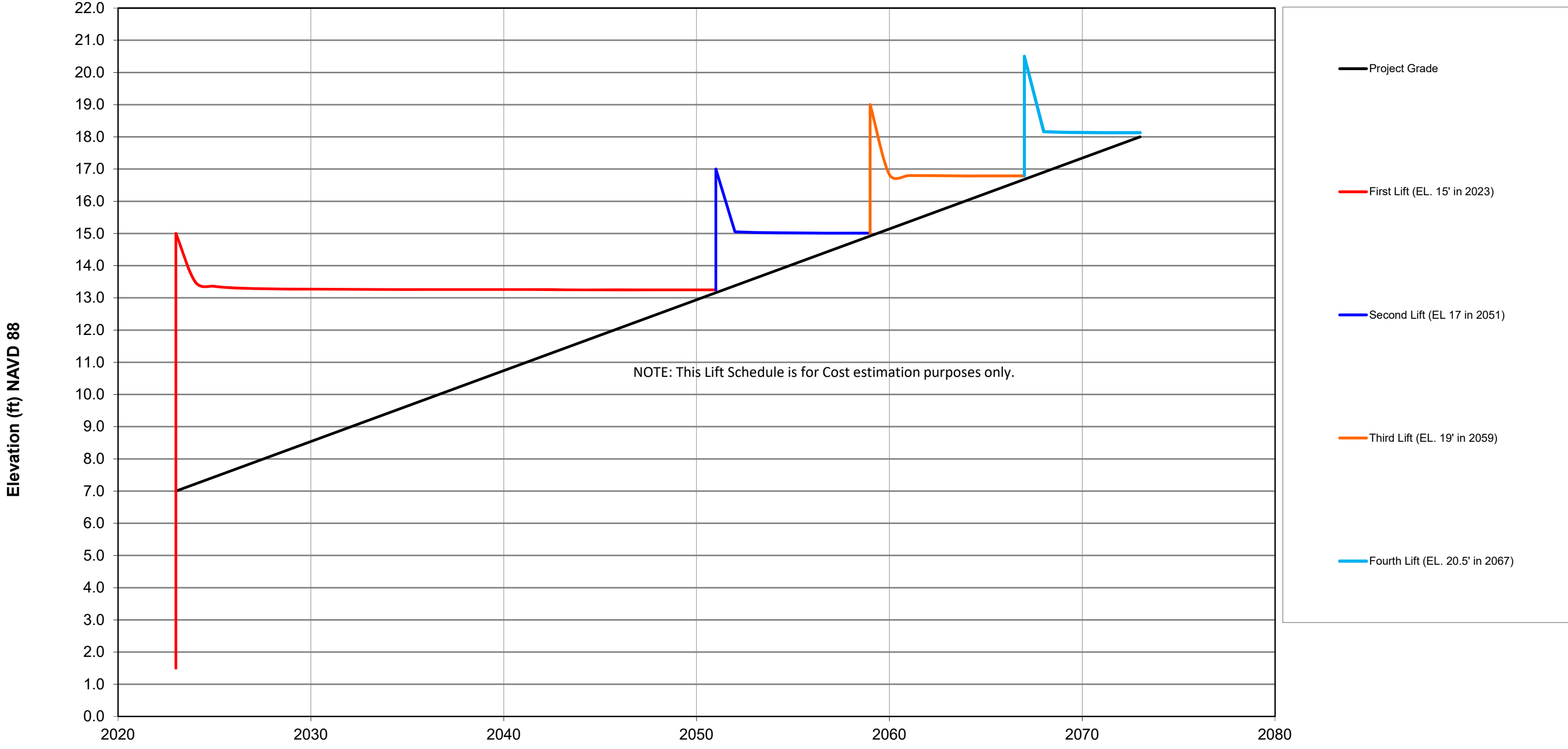
EL. 19' Upper Barataria Basin Section for Cost Estimation Purposes



EL. 21' Upper Barataria Basin Section for Cost Estimation Purposes

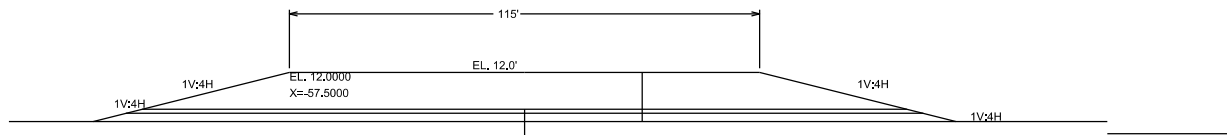
Alternative 6 - Reaches A, B, C, D, E, F, G, H, and K

Upper Barataria Basin Lift Schedule For Alternative 8 - Highway

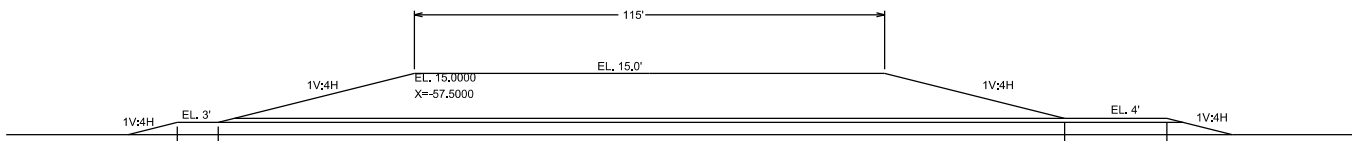


NOTE: This Lift Schedule is for Cost estimation purposes only.

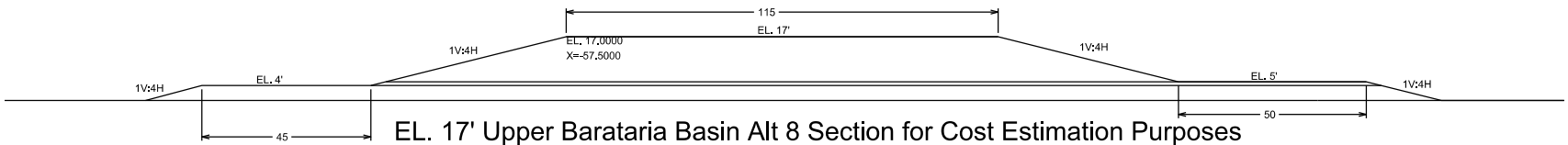
Note: Time-Rate Settlement Calculations are only an estimate. Time-Rate Settlement may vary from what is shown and is only developed for planning purposes.



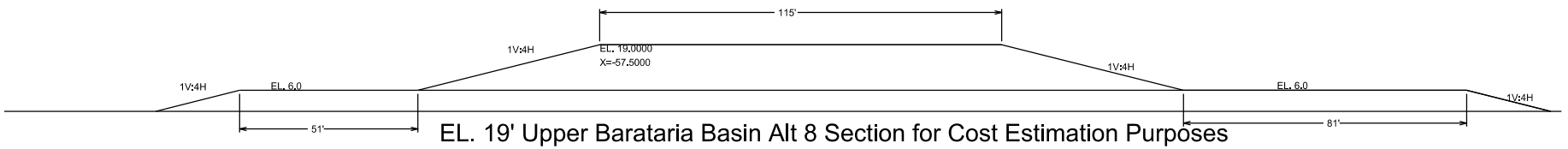
EL. 12' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



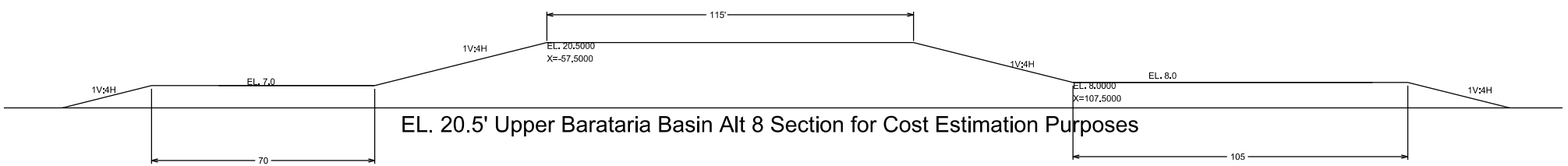
EL. 15' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



EL. 17' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



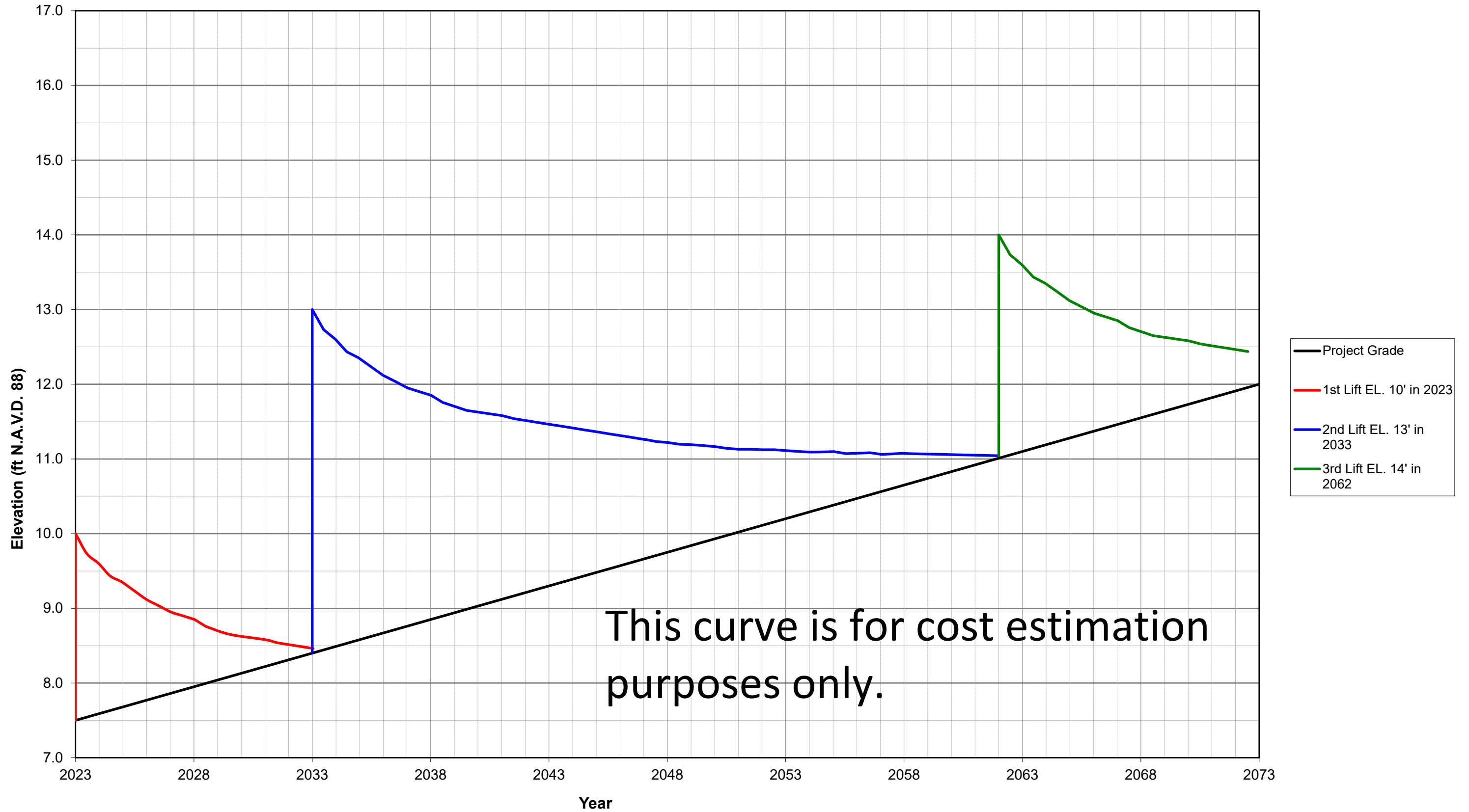
EL. 19' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes



EL. 20.5' Upper Barataria Basin Alt 8 Section for Cost Estimation Purposes

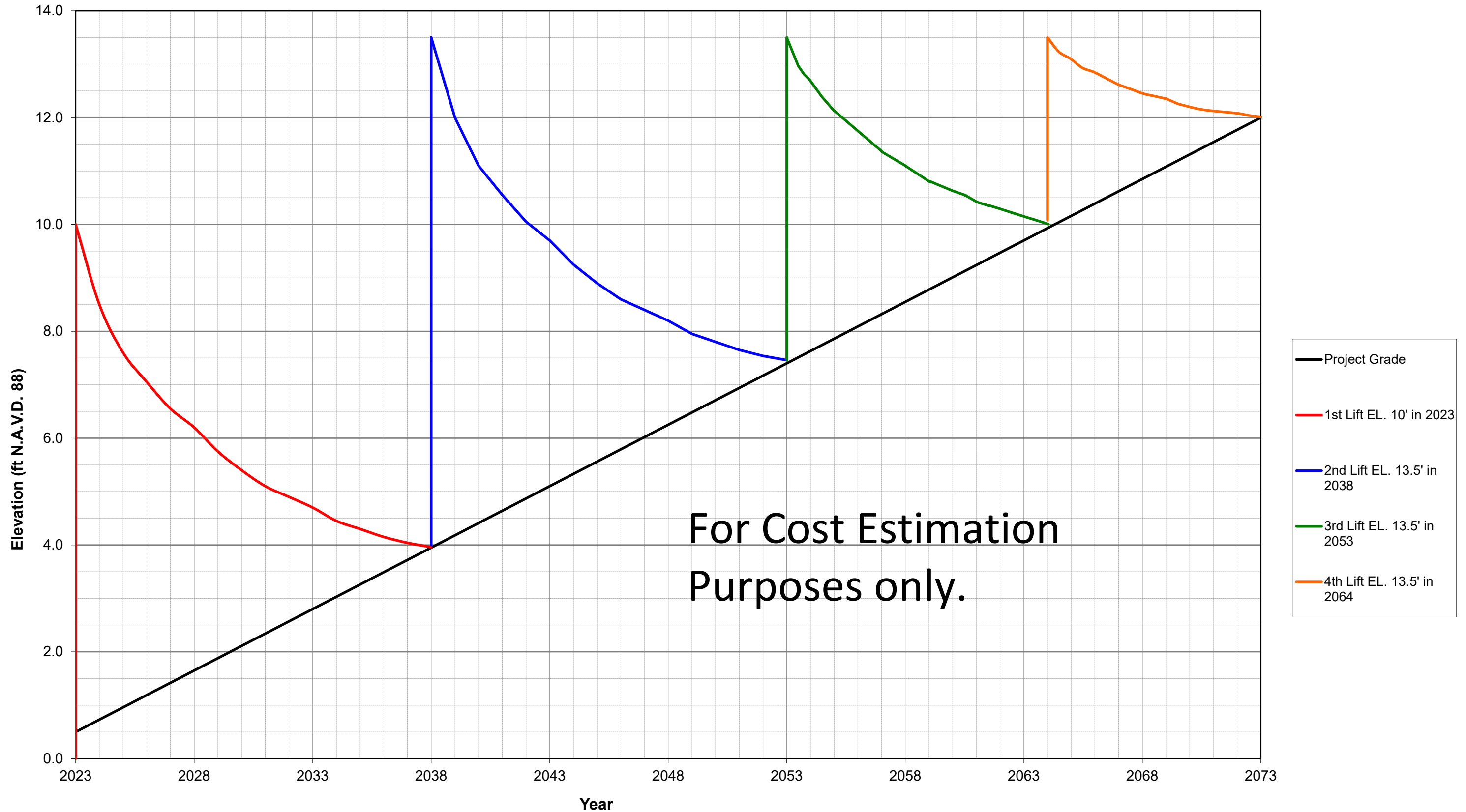
Alternative 8 - Reaches G, H, and I

Alternative 10
Upper Barataria Basin Reaches A,B and C- Lift Schedule

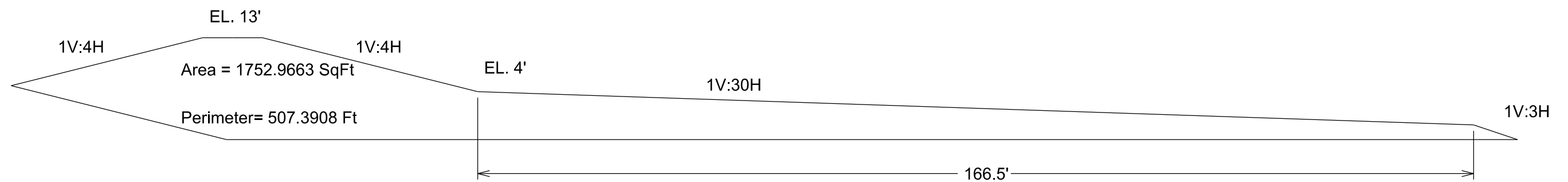


This curve is for cost estimation purposes only.

Upper Barataria Basin Reaches D to F - Lift Schedule



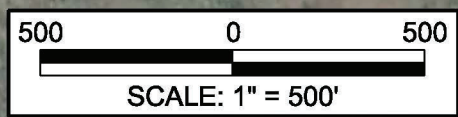
Typical Section used in the cost estimate to compare an alternative with a flood wall to a levee alternative




Typical Section from Appendix 8 of the Conceptual Design Report

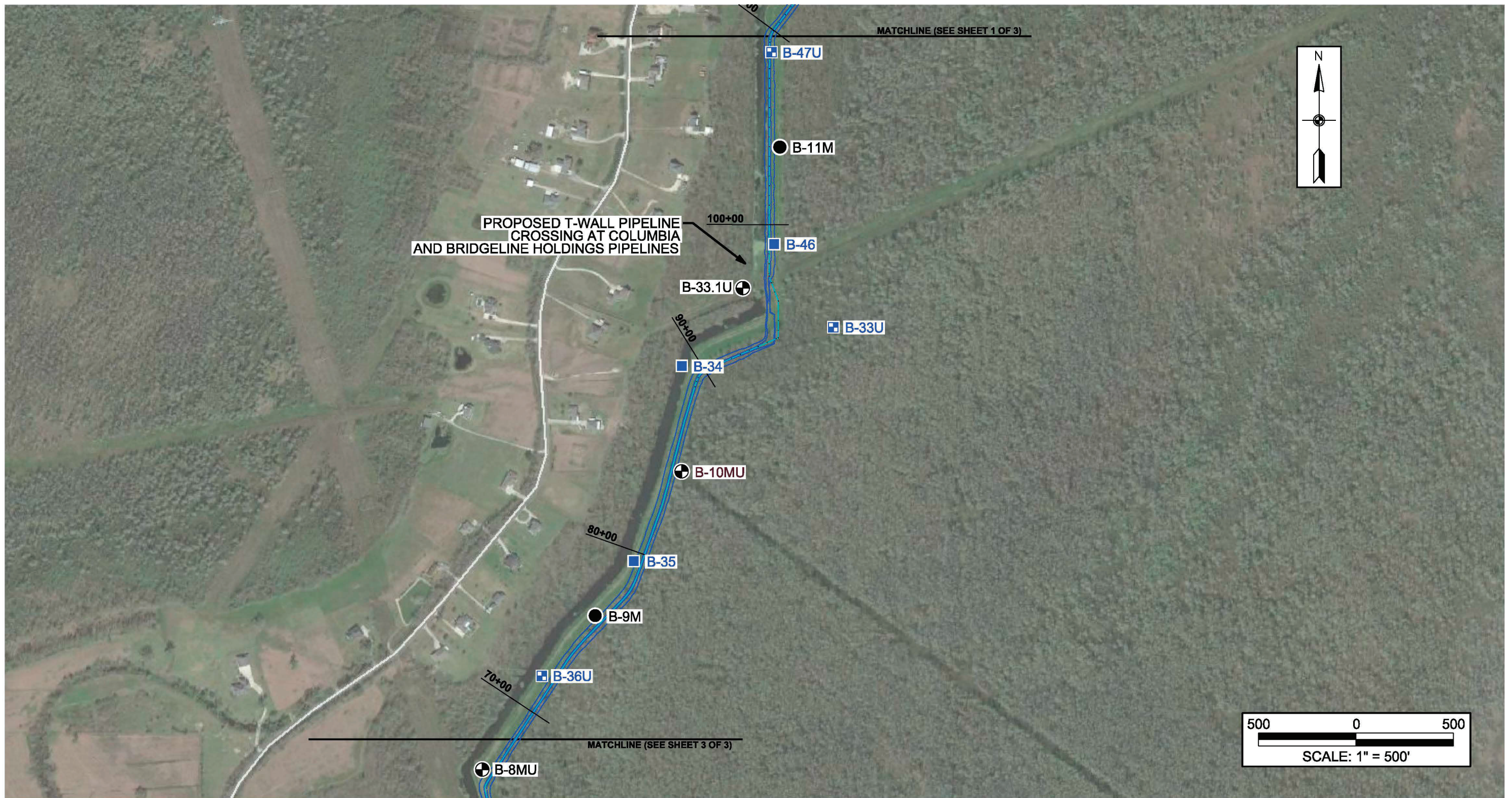
Upper Barataria Basin Risk Reduction
CPRA Project 002HP.06 Segment 2 Typical Section Segment 2

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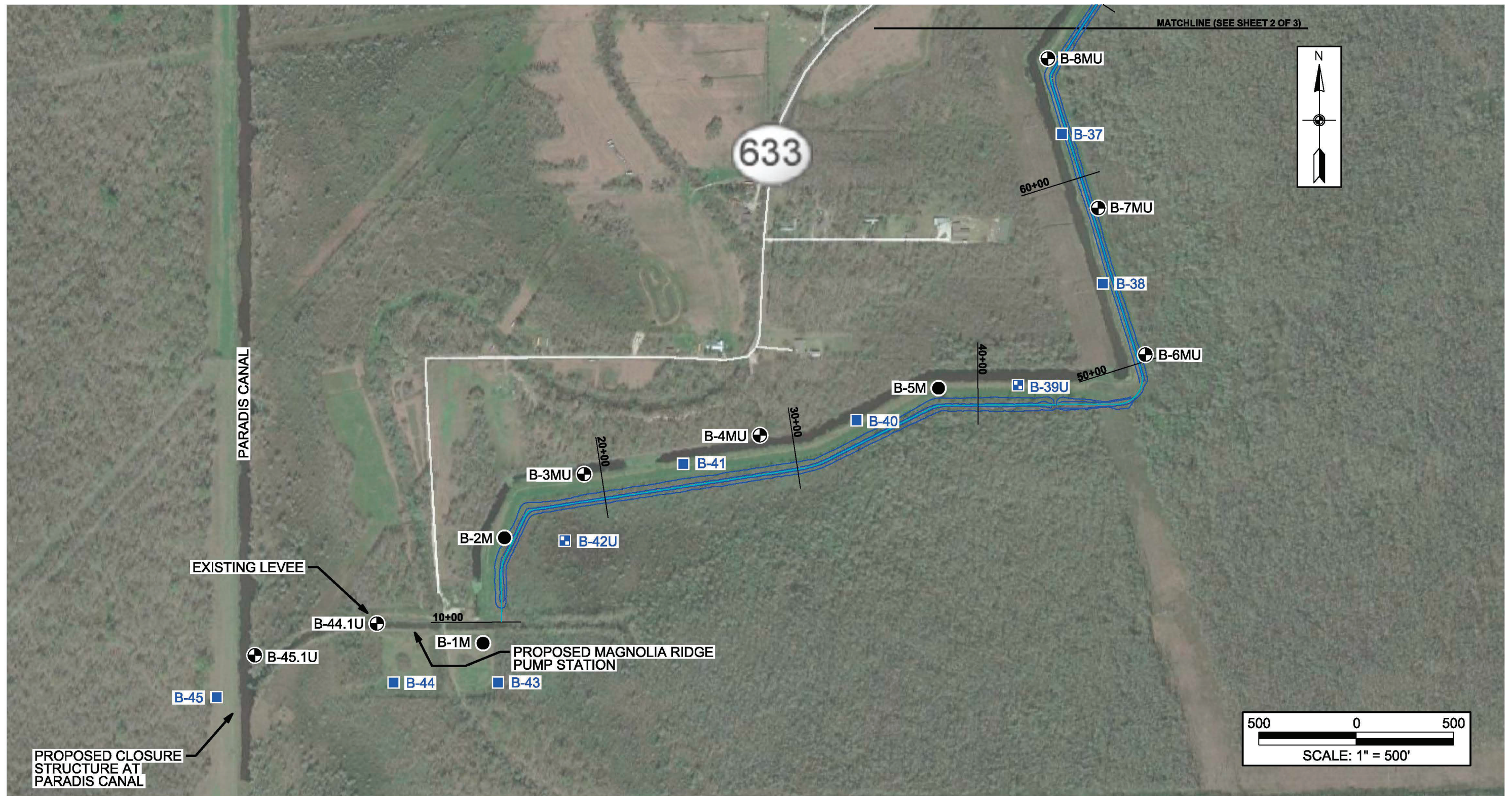
- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- ⊠ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995 AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995, 2003, AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194

| | | |
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| BORING LOCATION PLAN ST. CHARLES PARISH MAGNOLIA RIDGE LEVEE PROJECT REPORT I - EARTHEN LEVEES ST. CHARLES PARISH, LOUISIANA ST. CHARLES PARISH PROJECT NO. P080905-6A | | |
| DRAWN BY: J.L.S. | PLOT DATE: 12 NOV 15 | CADD FILE: REPORT_I_PLAN.DGN |
| CHECKED BY: S.G.W. | JOB NO.: 22557 | FIGURE 1 (SHEET 1 OF 3) |




- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- ⊞ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995 AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194
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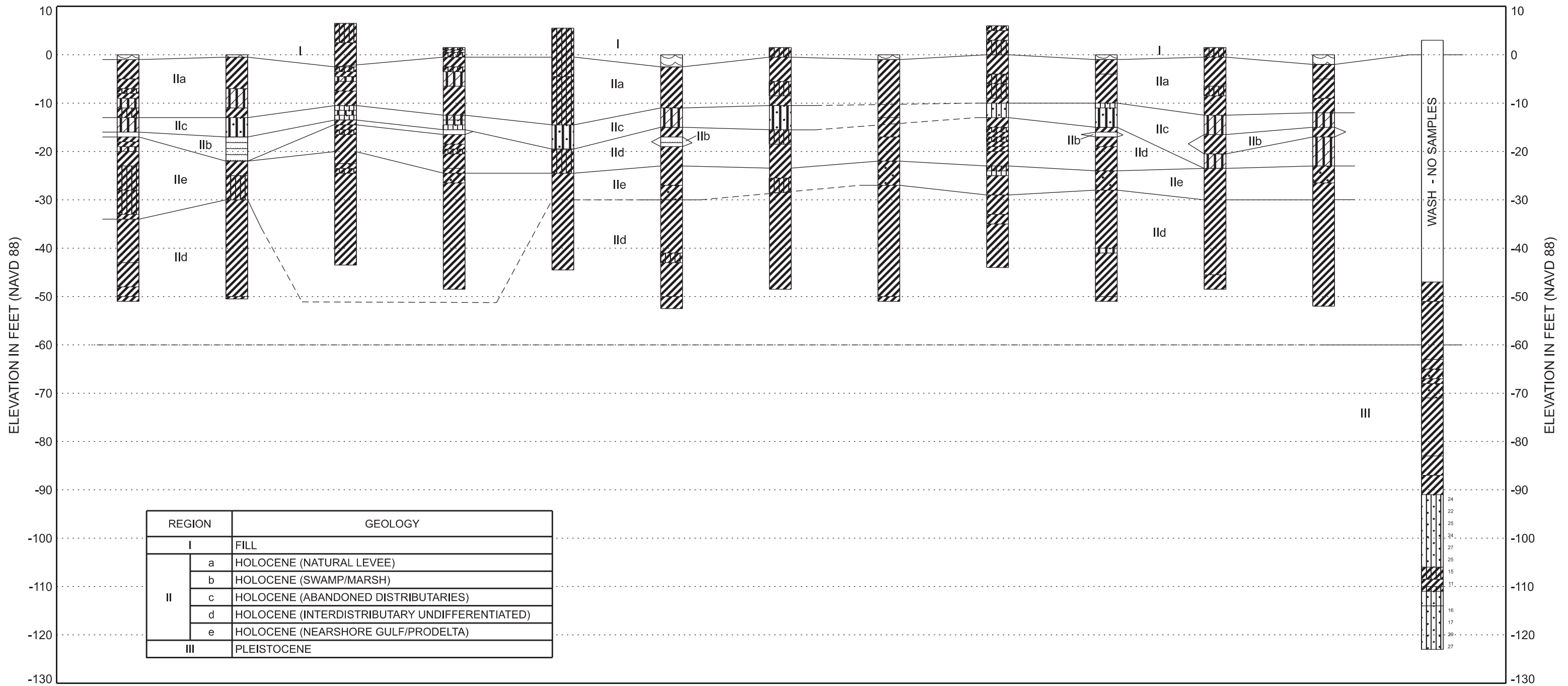
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| DRAWN BY: J.L.S. | PLOT DATE: 12 NOV 15 | CADD FILE: REPORT_I_PLAN.DGN |
| CHECKED BY: S.G.W. | JOB NO.: 22557 | FIGURE 1 (SHEET 2 OF 3) |



- ⊕ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- DENOTES APPROXIMATE LOCATIONS OF 3-IN. UNDISTURBED SOIL BORINGS DRILLED BETWEEN APRIL 2014 AND JUNE 2015 FOR THIS PROJECT
- ⊞ DENOTES APPROXIMATE LOCATIONS OF 5-IN. UNDISTURBED SOIL BORINGS DRILLED IN 1995 AND 2004 UNDER EUSTIS ENGINEERING PROJECT NO. 13194
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| <small>DRAWN BY: J.L.S.</small> | <small>PLOT DATE: 12 NOV 15</small> | <small>CADD FILE: REPORT_I_PLAN.DGN</small> |
| <small>CHECKED BY: S.G.W.</small> | <small>JOB NO.: 22557</small> | <small>FIGURE 1 (SHEET 3 OF 3)</small> |

| | | | | | | | | | | | | |
|--|---|---|---|--|---|---|---|---|--|--|---|---|
| B-51 04 NOV 04 29°53'28.98" -90°23'9.96" G.S.E. 0.00 | B-50 02 NOV 04 29°53'25.8" -90°23'17" G.S.E. 0.00 | B-16MU 16 JUN 14 29°53'18.78" -90°23'22.26" G.S.E. 6.50 | B-15MU 17 JUN 14 29°53'15.12" -90°23'25.92" G.S.E. 1.50 | B-14M 18 JUN 14 29°33'28.8" -90°23'29.4" G.S.E. 5.50 | B-49U 01 NOV 04 29°53'5.6" -90°23'30.4" G.S.E. 0.00 | B-13M 19 JUN 14 29°53'4.02" -90°23'35.82" G.S.E. 1.50 | B-48 29 OCT 04 29°52'59.6" -90°23'38.6" G.S.E. 0.00 | B-12MU 25 JUN 14 29°52'56.58" -90°23'41.88" G.S.E. 6.00 | B-47U 01 NOV 04 29°52'58.2" -90°23'43.9" G.S.E. 0.00 | B-11M 26 JUN 14 29°52'47.28" -90°23'44.16" G.S.E. 1.50 | B-46 01 NOV 04 29°52'42.2" -90°23'44.8" G.S.E. 0.00 | B-33.1U 18 MAY 15 29°52'39" -90°23'44.4001" G.S.E. 3.00 |
|--|---|---|---|--|---|---|---|---|--|--|---|---|



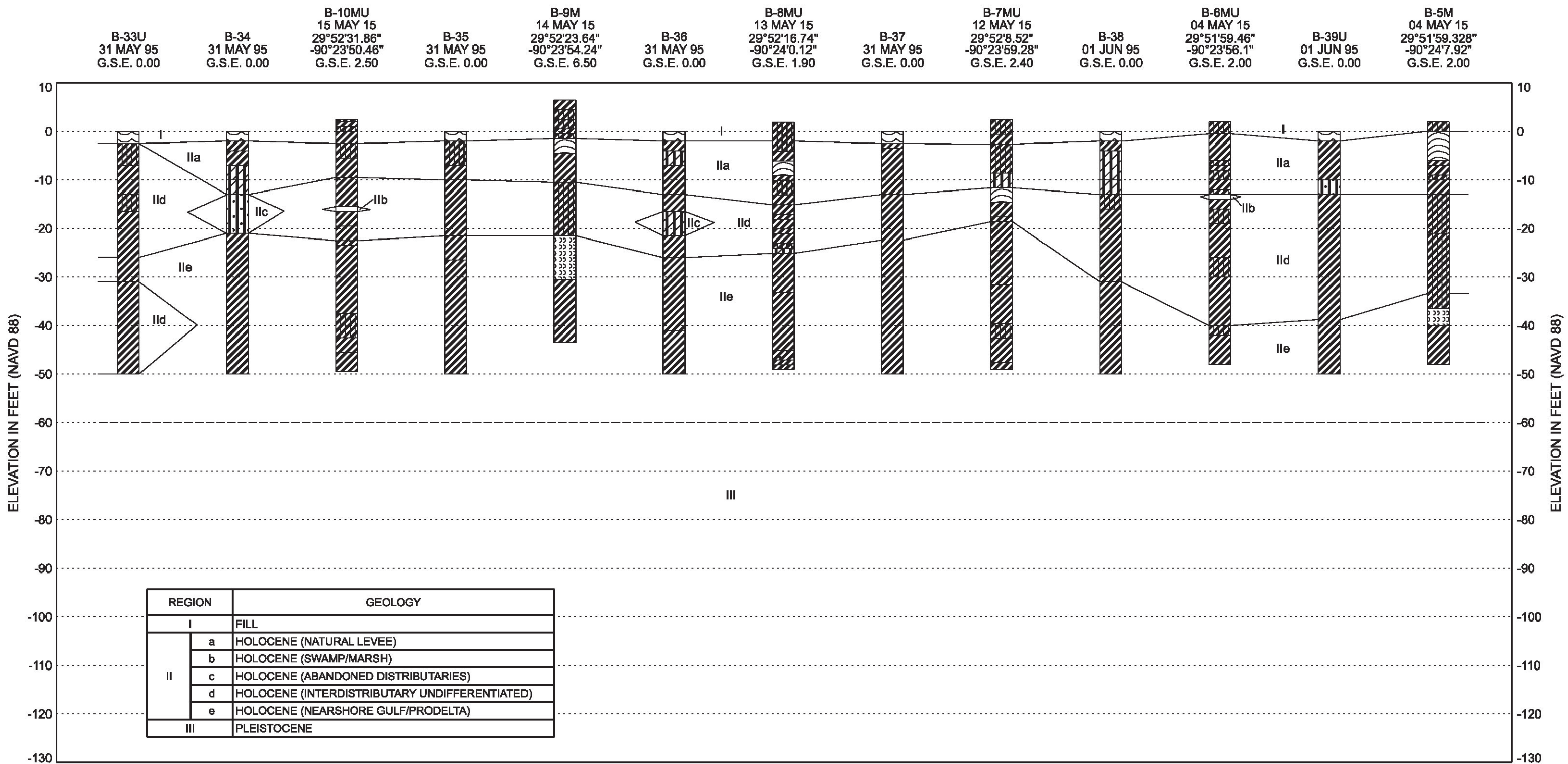
BORING MATERIAL GRAPHICS

- | | | |
|-------------|--------------|-------|
| CLAY | SANDY SILT | WATER |
| SILTY CLAY | CLAYEY SILT | |
| SANDY CLAY | ORGANIC CLAY | |
| SAND | PEAT/HUMUS | |
| SILTY SAND | WOOD | |
| CLAYEY SAND | SHELLS | |














NOTE:

NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").

| | | |
|--|----------------------|-------------------------|
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| <p>SUBSOIL PROFILE</p> <p>ST. CHARLES PARISH MAGNOLIA RIDGE LEVEE PROJECT REPORT I - EARTHEN LEVEES ST. CHARLES PARISH, LOUISIANA ST. CHARLES PARISH PROJECT NO. P080905-6A</p> | | |
| DRAWN BY: J.L.S. | PLOT DATE: 12 NOV 15 | CADD FILE: PROFILE.DGN |
| CHECKED BY: S.G.W. | JOB NO.: 22557 | FIGURE 2 (SHEET 1 OF 3) |




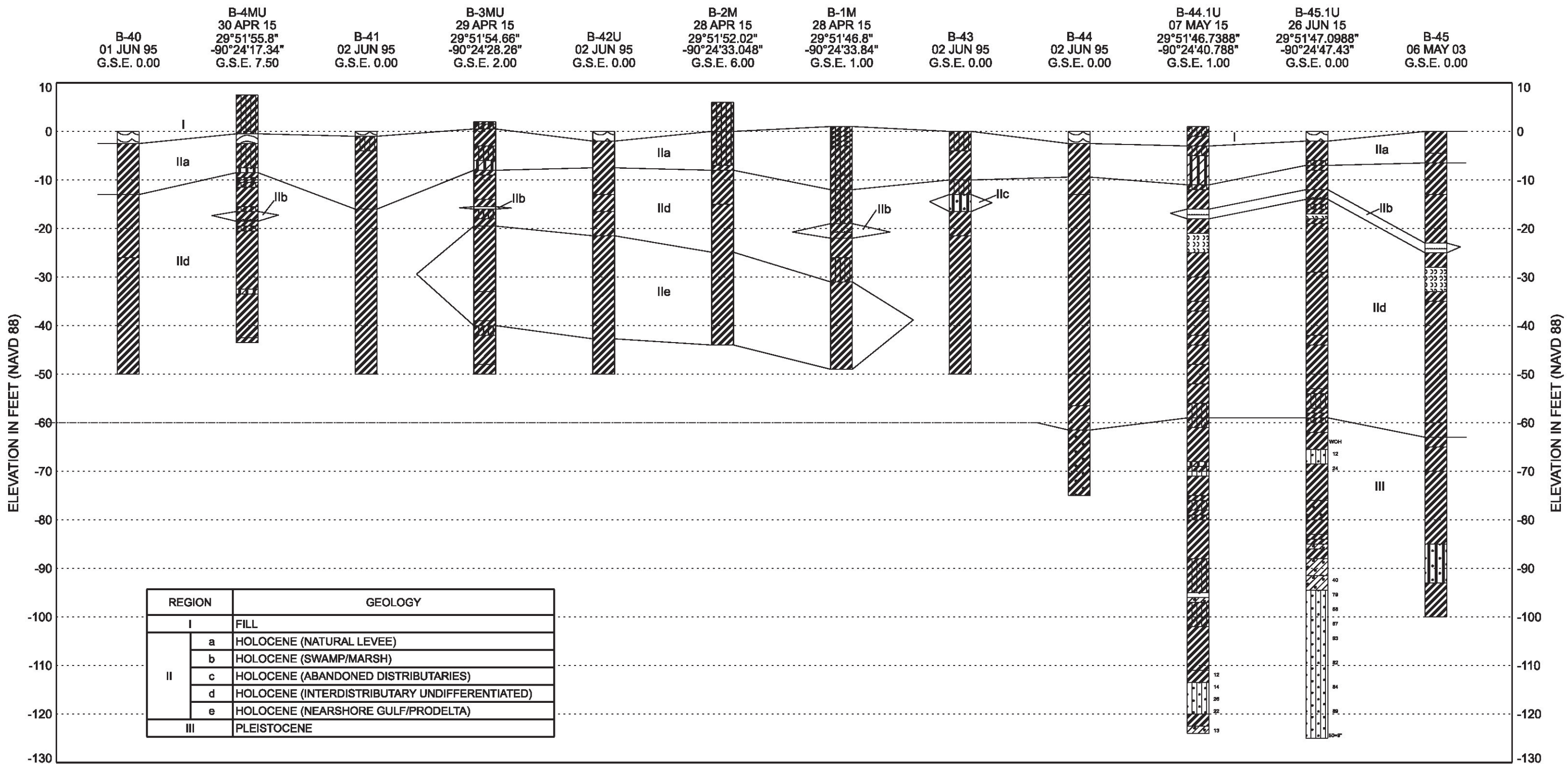
BORING MATERIAL GRAPHICS

-  CLAY
-  SILTY CLAY
-  SANDY CLAY
-  SAND
-  SILTY SAND
-  CLAYEY SAND
-  SANDY SILT
-  CLAYEY SILT
-  ORGANIC CLAY
-  PEAT/HUMUS
-  WOOD
-  SHELLS
-  WATER

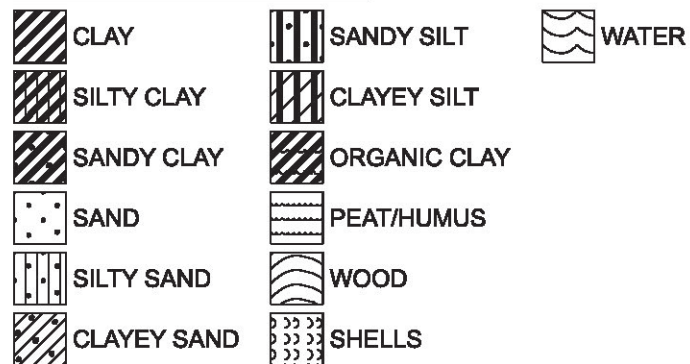
NOTE:

NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").

| | | |
|--|-------------------------------------|---|
|  | | |
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| SUBSOIL PROFILE | | |
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| <small>DRAWN BY: J.L.S.</small> | <small>PLOT DATE: 12 NOV 15</small> | <small>CADD FILE: PROFILE.DGN</small> |
| <small>CHECKED BY: S.G.W.</small> | <small>JOB NO.: 22557</small> | <small>FIGURE 2 (SHEET 2 OF 3)</small> |



BORING MATERIAL GRAPHICS



NOTE:

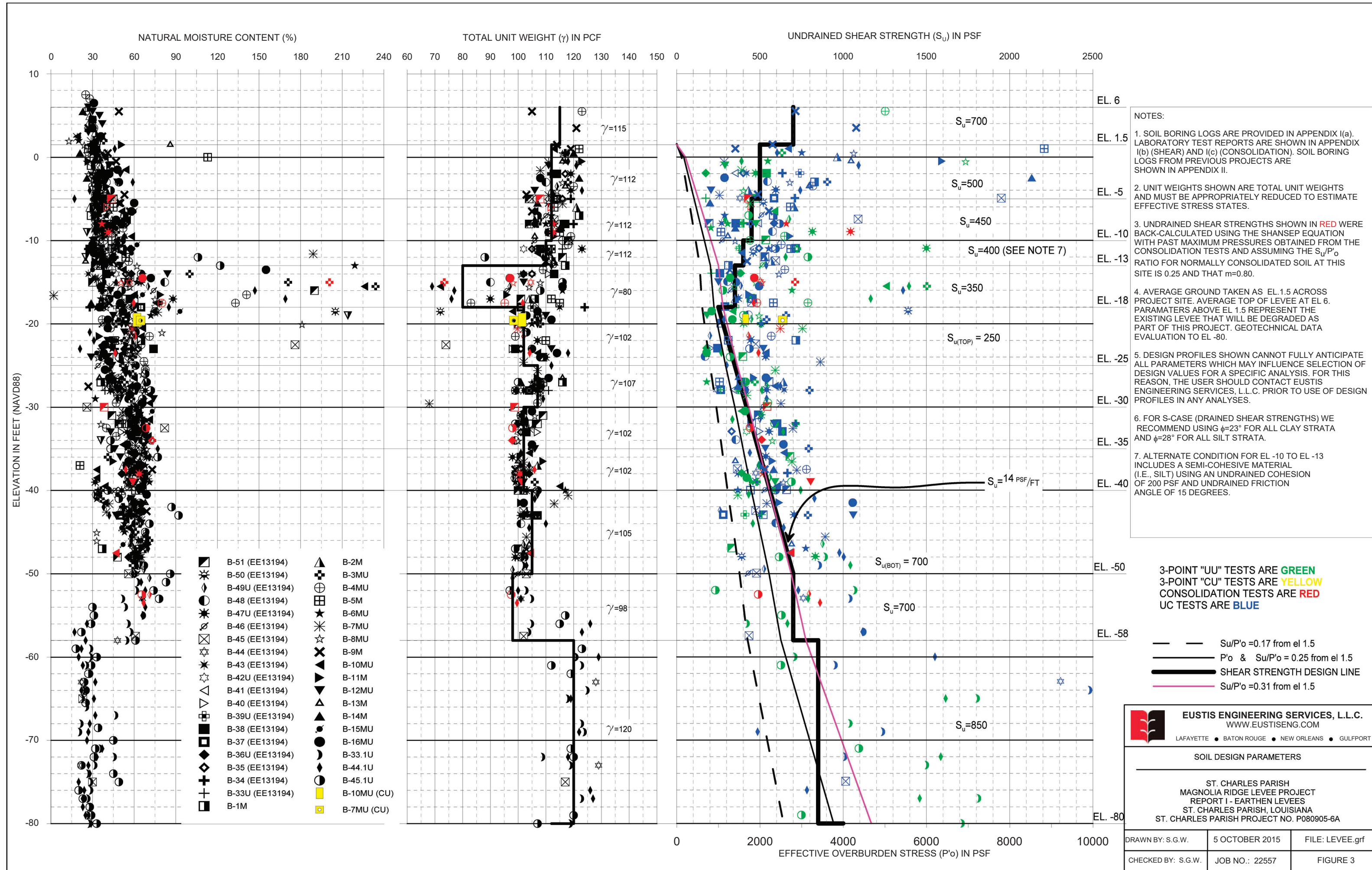
NUMBERS TO THE RIGHT OF THE BORING LOGS ARE STANDARD PENETRATION TEST (SPT) RESULTS (I.E., "N-VALUES").

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SUBSOIL PROFILE

ST. CHARLES PARISH
 MAGNOLIA RIDGE LEVEE PROJECT
 REPORT I - EARTHEN LEVEES
 ST. CHARLES PARISH, LOUISIANA
 ST. CHARLES PARISH PROJECT NO. P080905-6A

| | | |
|--------------------|----------------------|-------------------------|
| DRAWN BY: J.L.S. | PLOT DATE: 12 NOV 15 | CADD FILE: PROFILE.DGN |
| CHECKED BY: S.G.W. | JOB NO.: 22557 | FIGURE 2 (SHEET 3 OF 3) |



- NOTES:
1. SOIL BORING LOGS ARE PROVIDED IN APPENDIX I(a). LABORATORY TEST REPORTS ARE SHOWN IN APPENDIX I(b) (SHEAR) AND I(c) (CONSOLIDATION). SOIL BORING LOGS FROM PREVIOUS PROJECTS ARE SHOWN IN APPENDIX II.
 2. UNIT WEIGHTS SHOWN ARE TOTAL UNIT WEIGHTS AND MUST BE APPROPRIATELY REDUCED TO ESTIMATE EFFECTIVE STRESS STATES.
 3. UNDRAINED SHEAR STRENGTHS SHOWN IN RED WERE BACK-CALCULATED USING THE SHANSEP EQUATION WITH PAST MAXIMUM PRESSURES OBTAINED FROM THE CONSOLIDATION TESTS AND ASSUMING THE $S_u/P'0$ RATIO FOR NORMALLY CONSOLIDATED SOIL AT THIS SITE IS 0.25 AND THAT $m=0.80$.
 4. AVERAGE GROUND TAKEN AS EL.1.5 ACROSS PROJECT SITE. AVERAGE TOP OF LEVEE AT EL.6. PARAMETERS ABOVE EL.1.5 REPRESENT THE EXISTING LEVEE THAT WILL BE DEGRADED AS PART OF THIS PROJECT. GEOTECHNICAL DATA EVALUATION TO EL.-80.
 5. DESIGN PROFILES SHOWN CANNOT FULLY ANTICIPATE ALL PARAMETERS WHICH MAY INFLUENCE SELECTION OF DESIGN VALUES FOR A SPECIFIC ANALYSIS. FOR THIS REASON, THE USER SHOULD CONTACT EUSTIS ENGINEERING SERVICES, L.L.C. PRIOR TO USE OF DESIGN PROFILES IN ANY ANALYSES.
 6. FOR S-CASE (DRAINED SHEAR STRENGTHS) WE RECOMMEND USING $\phi=23^\circ$ FOR ALL CLAY STRATA AND $\phi=28^\circ$ FOR ALL SILT STRATA.
 7. ALTERNATE CONDITION FOR EL.-10 TO EL.-13 INCLUDES A SEMI-COHESIVE MATERIAL (I.E., SILT) USING AN UNDRAINED COHESION OF 200 PSF AND UNDRAINED FRICTION ANGLE OF 15 DEGREES.

- 3-POINT "UU" TESTS ARE GREEN
 - 3-POINT "CU" TESTS ARE YELLOW
 - CONSOLIDATION TESTS ARE RED
 - UC TESTS ARE BLUE
- $S_u/P'0 = 0.17$ from el.1.5
 - $P'0$ & $S_u/P'0 = 0.25$ from el.1.5
 - SHEAR STRENGTH DESIGN LINE
 - $S_u/P'0 = 0.31$ from el.1.5

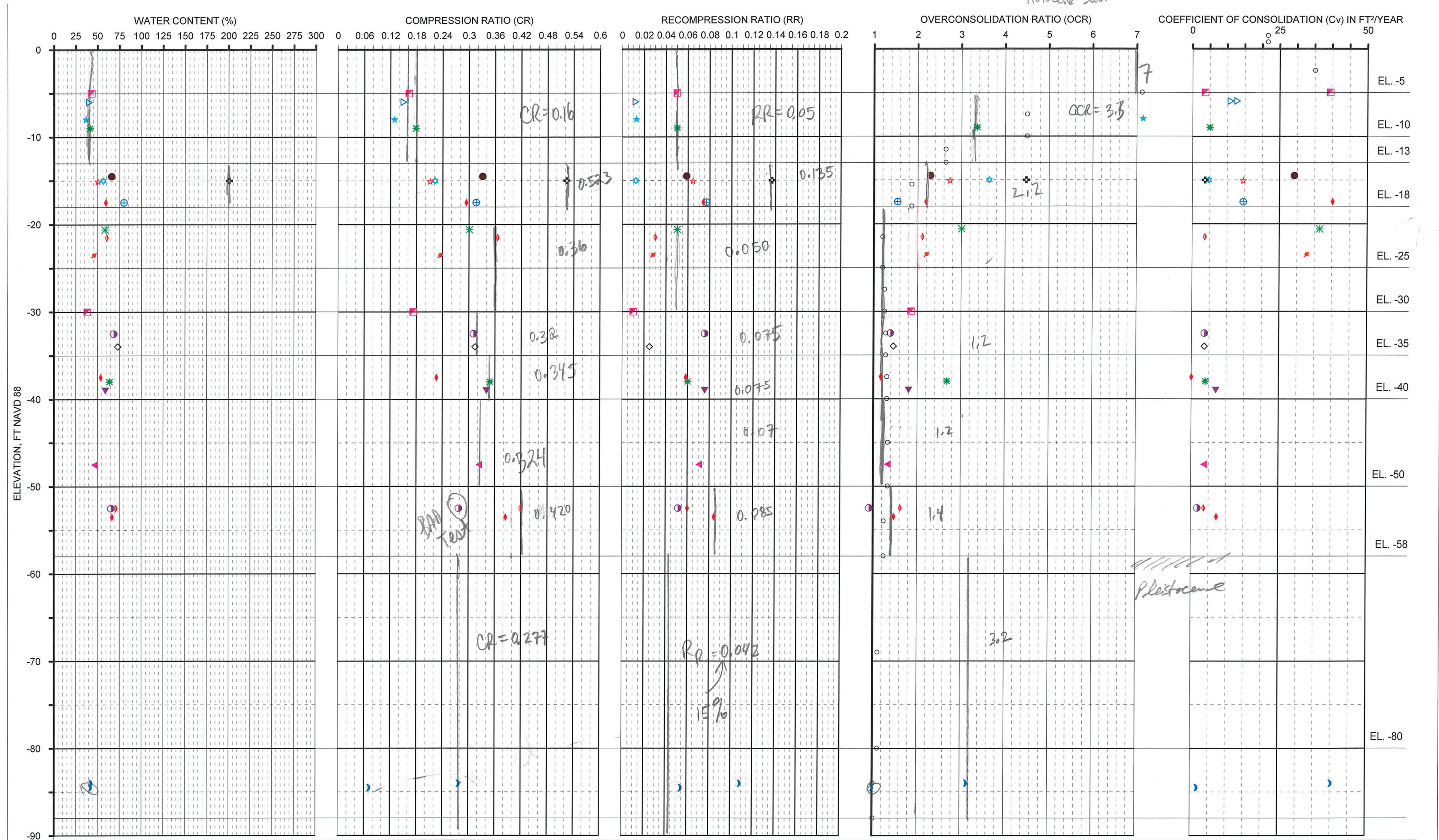
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SOIL DESIGN PARAMETERS

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 REPORT I - EARTHEN LEVEES
 ST. CHARLES PARISH, LOUISIANA
 ST. CHARLES PARISH PROJECT NO. P080905-6A

| | | |
|--------------------|----------------|-----------------|
| DRAWN BY: S.G.W. | 5 OCTOBER 2015 | FILE: LEVEE.grf |
| CHECKED BY: S.G.W. | JOB NO.: 22557 | FIGURE 3 |

Holocene shouldn't use ocr > 1.1 (???)



| | | | | | | | | | | | | | | | | | | | |
|---|-----------|---|-------------|---|-------------|---|--------------|---|--------------|---|-------------------|---|---------------------|---|---------------------|---|--------------------|---|---------------------|
| + | B-3MU, 6B | * | B-7MU, 8C | ▼ | B-12MU, 13B | ☾ | B-33.1U, 10B | ◆ | B-44.1U, 11C | ◐ | B-45.1U, 13C | ☆ | B-44, 5 (EE13194) | * | B-47, 3B (EE13194) | ◆ | B-49, 5C (EE13194) | ◻ | B-51, 8C (EE13194) |
| ⊕ | B-4MU, 9B | ☆ | B-8MU, 6C | ◐ | B-15MU, 8B | ☾ | B-33.1U, 10B | ◆ | B-44.1U, 15C | ◐ | B-35, 9 (EE13194) | * | B-47, 10C (EE13194) | ◆ | B-49, 13C (EE13194) | ◻ | B-51, 2B (EE13194) | ○ | SHANSEP OCR |
| ★ | B-6MU, 4C | ◀ | B-10MU, 14C | ● | B-16MU, 7B | ◆ | B-44.1U, 6C | ◐ | B-45.1U, 8C | ◁ | B-40, 2 (EE13194) | | | | | | | | $m=0.8$ $c=0.25$ |

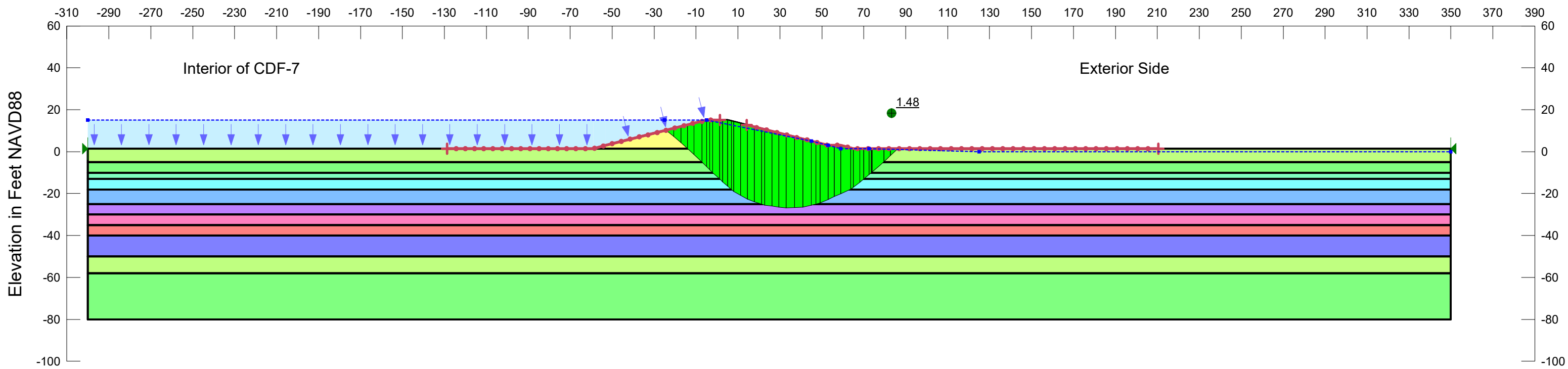
EE 22557
Magnolia Ridge
Consolidation Test Summary

Homogeneous CL and CH sedimentary clays of low to moderate sensitivity ($I_p = 20\% - 80\%$):
 $S = 0.20 + 0.05I_p$, or simply $S = 0.22$.
 $m = 0.88(1 - C_c/C_c) \pm 0.06 SD$, or simply $m = 0.8$.
 Sedimentary deposits of silts and organic soils (Atterberg limits plot below the A-line, but excluding peats) and clays with shells:
 $S = 0.25$, with nominal $SD = 0.05$.
 $m = 0.88(1 - C_c/C_c) \pm 0.06 SD$, or simply $m = 0.8$.

$$\frac{C_u}{\sigma'_{1\%}} = S(OCR)^m$$

0.8 = m
0.25 = S

| No. | Boring | Sample | Boring El. (feet) | Sample Depth (feet) | Sample El. (feet) | USCS | w% | Cc | Cs | eo | CR | RR Based on Consol Test | Theoretical RR=.15*CR | Dry Unit Weight (pcf) | Moist Unit Weight (pcf) | Approximate P'o (Psf) | Approximate P'o (tsf) | Approximate P'c (tsf) | OCR = P'o/P'o | S _u = P'o*S*(P' _{cr}) ^m | C _v (sq.ft/year) | Remarks | |
|-----|--------|----------------|-------------------|---------------------|-------------------|------|-------|-------|-------|-------|-------|-------------------------|-----------------------|-----------------------|-------------------------|-----------------------|-----------------------|-----------------------|---------------|---|-----------------------------|---------|------------------|
| 1 | B12MU | 13B | 6.0 | 45.0 | -39.0 | CH | 59.1 | 0.911 | 0.202 | 1.674 | 0.341 | 0.076 | 0.051 | 63.6 | 101.2 | 2005.0 | 1.00 | 1.81 | 1.81 | 804 | 45 | 7.00 | 591 |
| 2 | B15MU | 8B | 1.5 | 25.0 | -23.5 | CH | 46.3 | 0.628 | 0.075 | 1.674 | 0.235 | 0.028 | 0.035 | 71.2 | 104.2 | 1042.0 | 0.52 | 1.15 | 2.21 | 491 | 60 | 32.85 | 268 |
| 3 | B16MU | 7B | 6.5 | 21.0 | -14.5 | CH | 66.0 | 0.968 | 0.171 | 1.925 | 0.331 | 0.059 | 0.050 | 58.5 | 97.1 | 960.6 | 0.48 | 1.10 | 2.29 | 466 | 73 | 29.20 | 320 |
| 4 | B3MU | 6B | 2.0 | 17.0 | -15.0 | OH | 200.8 | 3.279 | 0.858 | 5.268 | 0.523 | 0.137 | 0.078 | 24.4 | 73.4 | 856.2 | 0.43 | 1.92 | 4.48 | 711 | 18 | 3.65 | 1503 |
| 5 | B4MU | 9B | 7.5 | 25.0 | -17.5 | OH | 79.9 | 0.989 | 0.240 | 2.126 | 0.316 | 0.077 | 0.047 | 52.9 | 95.2 | 1363.0 | 0.68 | 1.05 | 1.54 | 482 | 29 | 14.60 | 788 |
| 6 | B6MU | 4C | 2.0 | 10.0 | -8.0 | CL | 36.7 | 0.264 | 0.026 | 1.044 | 0.129 | 0.012 | 0.019 | 82.5 | 112.8 | 546.0 | 0.27 | 1.95 | 7.14 | 658 | 365 | 365.00 | 306/205 |
| 7 | B7MU | 8C | 2.4 | 23.0 | -20.6 | CH | 58.6 | 0.807 | 0.134 | 1.680 | 0.301 | 0.050 | 0.045 | 62.9 | 99.8 | 1030.0 | 0.52 | 1.55 | 3.01 | 622 | 219 | 36.50 | CU=381; UU=755 |
| 8 | B8MU | 6C | 1.9 | 17.0 | -15.1 | CH | 50.4 | 0.549 | 0.168 | 1.602 | 0.211 | 0.064 | 0.032 | 65.3 | 98.2 | 912.2 | 0.46 | 1.25 | 2.74 | 511 | 29 | 14.60 | 475 |
| 9 | B10MU | 14C | 2.5 | 50.0 | -47.5 | CH | 46.9 | 0.779 | 0.170 | 1.405 | 0.324 | 0.071 | 0.049 | 71.1 | 104.4 | 2181.0 | 1.09 | 1.45 | 1.33 | 685 | 32 | 3.65 | 679 |
| 10 | B33.1U | 10B 3' test | 3.0 | 87.0 | -84.0 | CH | 42.4 | 0.598 | 0.234 | 1.159 | 0.277 | 0.108 | 0.042 | 78.7 | 112.1 | 4205.2 | 2.10 | 6.60 | 3.14 | 2625 | | 40.15 | uu=1561/1846(Uc) |
| 11 | B33.1U | * 10B BAD TEST | 3.0 | 87.5 | -84.5 | CH | 41.7 | 0.153 | 0.116 | 1.142 | 0.071 | 0.054 | 0.011 | 79.3 | 112.4 | 4205.2 | 2.10 | 2.08 | 0.99 | 1042 | 29 | 1.83 | uu=1561; 1846=Uc |
| 12 | B44.1U | 6C | 1.0 | 18.5 | -17.5 | OH | 59.6 | 0.749 | 0.189 | 1.548 | 0.294 | 0.074 | 0.044 | 63.7 | 101.7 | 985.6 | 0.49 | 1.08 | 2.19 | 462 | 40 | 40.15 | 1165 |
| 13 | B44.1U | 11C | 1.0 | 38.5 | -37.5 | CH | 53.9 | 0.558 | 0.144 | 1.466 | 0.226 | 0.058 | 0.034 | 68.8 | 105.9 | 1881.0 | 0.94 | 1.10 | 1.17 | 533 | 29 | 0.00 | 492 |
| 14 | B44.1U | 15C | 1.0 | 54.5 | -53.5 | CH | 66.8 | 1.103 | 0.242 | 1.866 | 0.385 | 0.084 | 0.058 | 59.7 | 99.6 | 2526.5 | 1.26 | 1.86 | 1.47 | 861 | 22 | 3.65 | 1460 |
| 15 | B45.1U | 8C | 0.0 | 32.5 | -32.5 | CH | 68.6 | 0.908 | 0.220 | 1.922 | 0.311 | 0.075 | 0.047 | 58.1 | 98.0 | 1356.0 | 0.68 | 0.94 | 1.39 | 440 | 40 | 3.65 | 588 |
| 16 | B45.1U | * 13C | 0.0 | 52.5 | -52.5 | CH | 65.5 | 0.806 | 0.149 | 1.904 | 0.278 | 0.051 | 0.042 | 58.9 | 97.5 | 2108.0 | 1.05 | 0.96 | 0.91 | 489 | N/A | 1.83 | 232 |
| 24 | B35 | 9 | 0.0 | 34.0 | -34.0 | CH | 73.0 | 0.950 | | 2.023 | 0.314 | 0.025 | 0.047 | 56.6 | 97.9 | 1513.0 | 0.76 | 1.10 | 1.45 | 510 | 7.3 | 3.65 | |
| 25 | B40 | 2 | 0.0 | 6.0 | -6.0 | CH | 40.6 | 0.320 | | 1.134 | 0.150 | 0.012 | 0.022 | 79.6 | 111.9 | 301.0 | 0.15 | 1.40 | 9.30 | 448 | 18 | 10.95 | |
| 26 | B44 | 5 | 0.0 | 15.0 | -15.0 | CH | 56.5 | 0.570 | | 1.562 | 0.222 | 0.012 | 0.033 | 66.8 | 104.5 | 715.0 | 0.36 | 1.30 | 3.64 | 502 | 9 | 4.75 | |
| 27 | B47 | 3B | 0.0 | 9.0 | -9.0 | CH | 41.4 | 0.380 | | 1.130 | 0.178 | 0.050 | 0.027 | 79.7 | 112.7 | 441.0 | 0.79 | 2.66 | 3.35 | 1044 | 26 | 5.00 | |
| 28 | B47 | 10C | 0.0 | 38.0 | -38.0 | CH | 63.7 | 0.970 | | 1.781 | 0.349 | 0.060 | 0.052 | 61.5 | 100.7 | 1587.0 | 0.47 | 1.27 | 2.68 | 521 | / | 4.00 | |
| 29 | B49 | 5C | 0.0 | 21.5 | -21.5 | CH | 60.7 | 0.980 | | 1.679 | 0.366 | 0.030 | 0.055 | 63.4 | 101.9 | 948.0 | 0.47 | 1.00 | 2.11 | 431 | 22 | 3.65 | |
| 30 | B49 | 13C | 0.0 | 52.5 | -52.5 | CH | 71.1 | 1.250 | | 1.980 | 0.419 | 0.060 | 0.063 | 57.4 | 98.2 | 2166.5 | 1.08 | 1.75 | 1.62 | 795 | 48 | 3.65 | |
| 31 | B51 | 2B | 0.0 | 5.0 | -5.0 | CH | 43.5 | 0.370 | | 1.276 | 0.163 | 0.050 | 0.024 | 75.2 | 107.9 | 245.0 | 0.12 | 1.40 | 11.43 | 430 | 44 | 3.65 | |
| 32 | B51 | 8C | 0.0 | 30.0 | -30.0 | CL | 38.4 | 0.360 | | 1.084 | 0.173 | 0.010 | 0.026 | 71.3 | 98.7 | 1325.0 | 0.66 | 1.23 | 1.86 | 543 | 923 | 146.00 | |



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GENERAL NOTES

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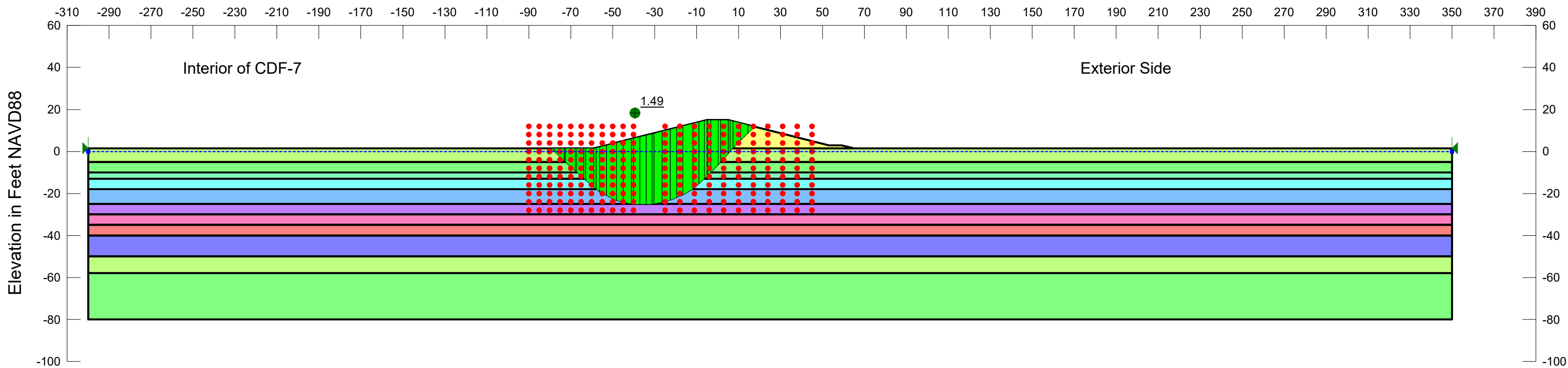
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Construction Grade - Entry Exit Slip Surface
 Louisiana



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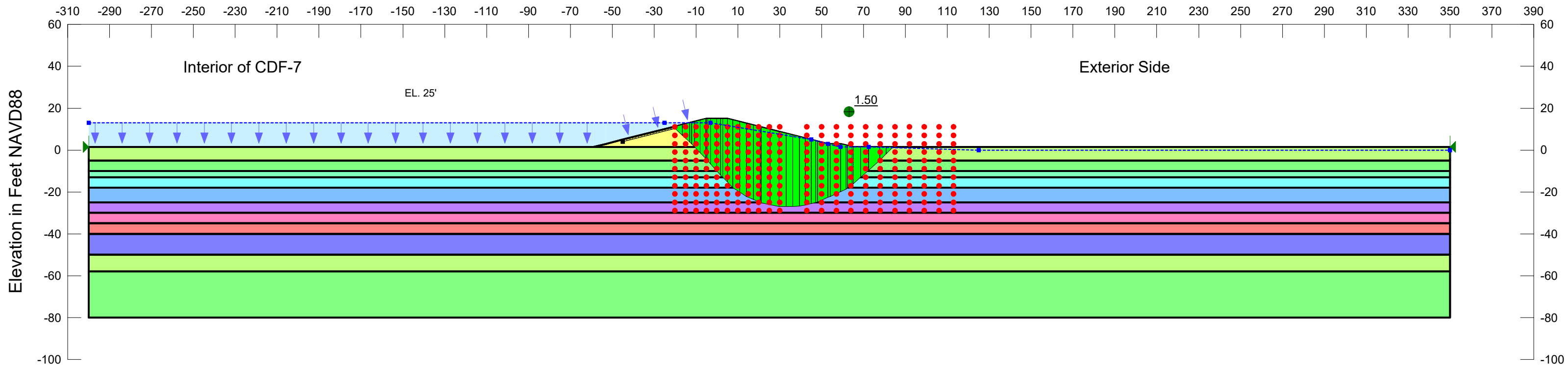
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Low Water Level - Block Slip Surface
 Louisiana



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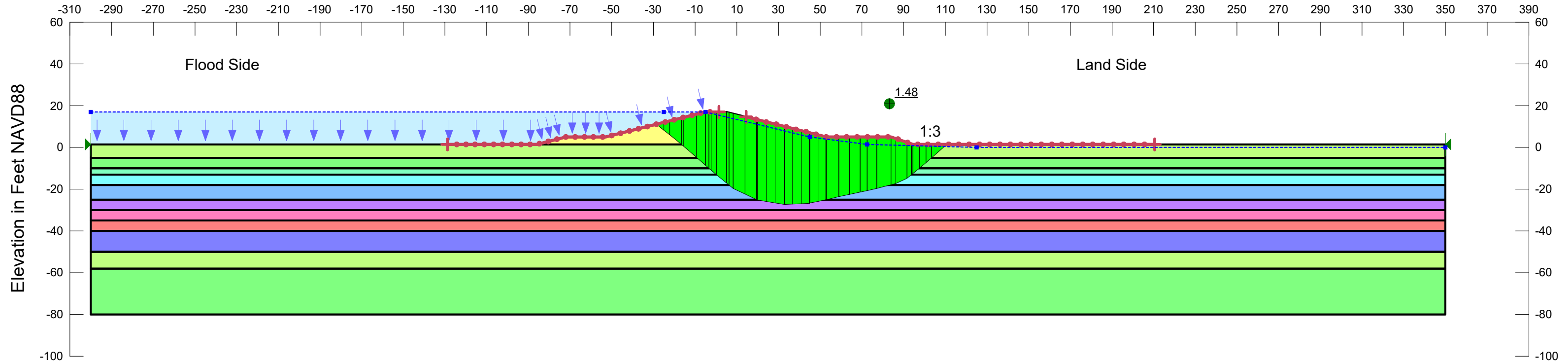
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Still Water Level - Block Slip Surface
 Louisiana



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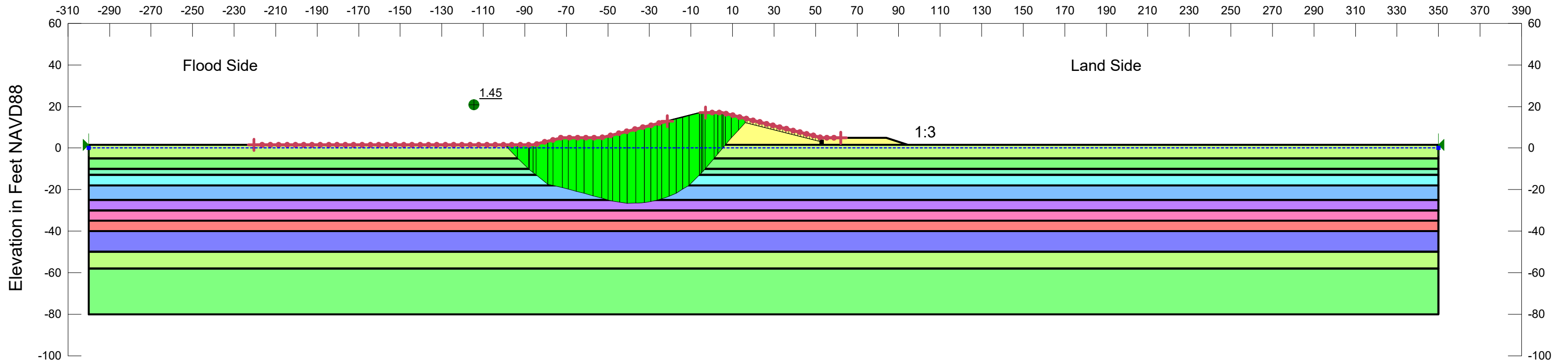
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Top of Levee - Entry Exit Slip Surface
 Louisiana



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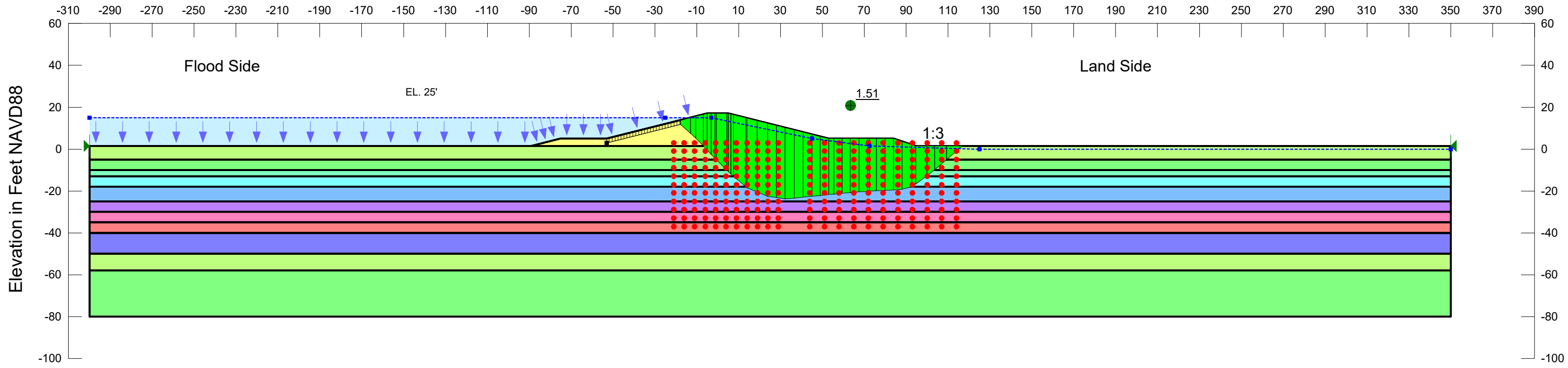
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Low Water Level - Entry Exit Slip Surface
 Louisiana



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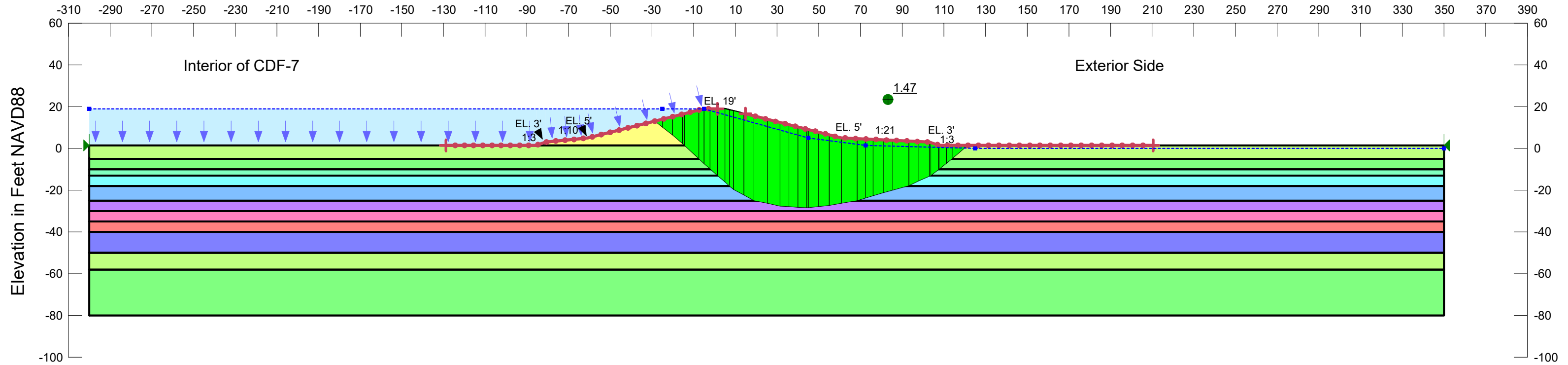
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Still Water Level - Block Slip Surface
 Louisiana



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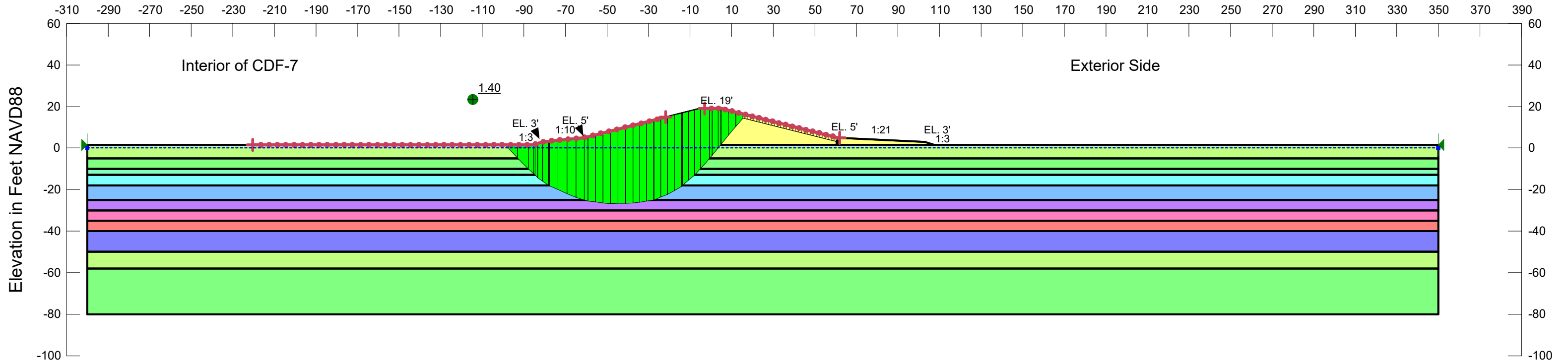
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Top of Levee - Entry Exit Slip Surface
 Louisiana



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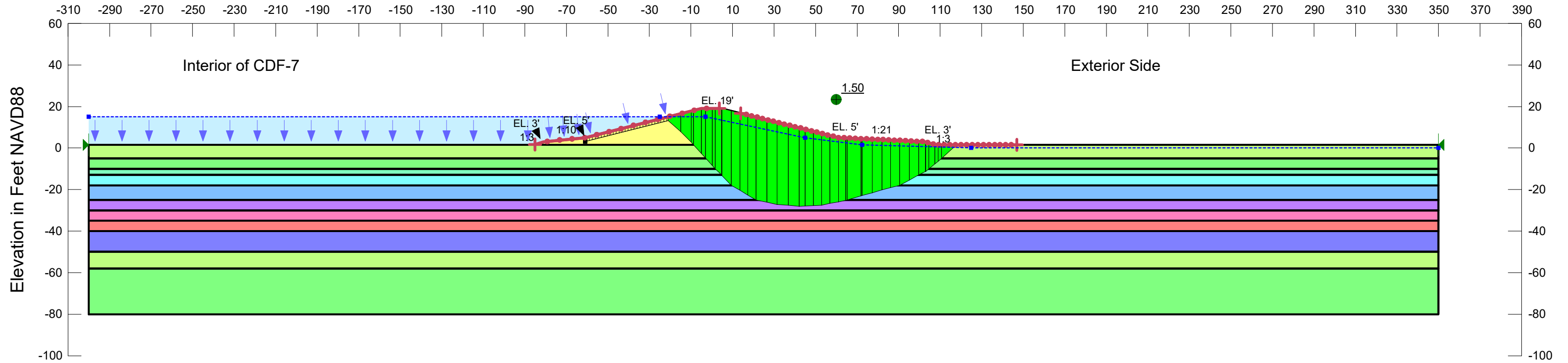
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Low Water Level - Entry Exit Slip Surface
 Louisiana



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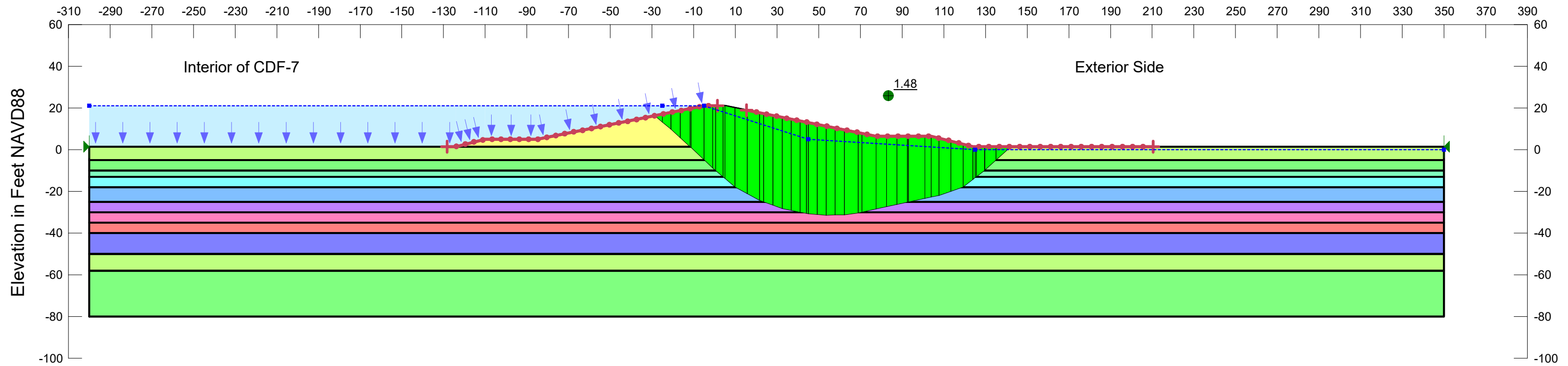
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Still Water Level - Entry Exit Slip Surface
 Louisiana



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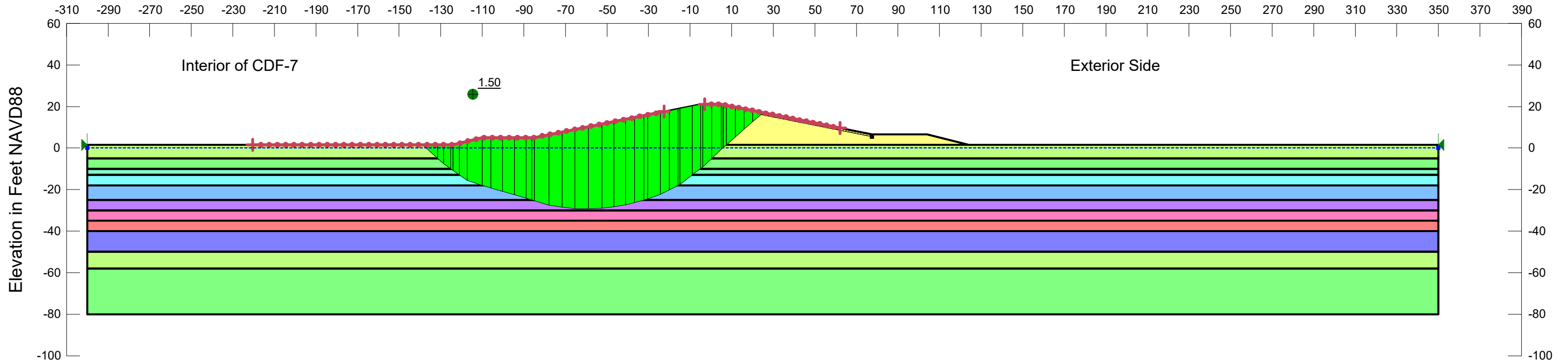
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 On page 29/113 of Appendix 4-Geotechnical Investigations Figure 2.2. from the
 LBLD -Upper Barataria RRP Conceptual Report
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Top of Levee - Entry Exit Slip Surface
 Louisiana



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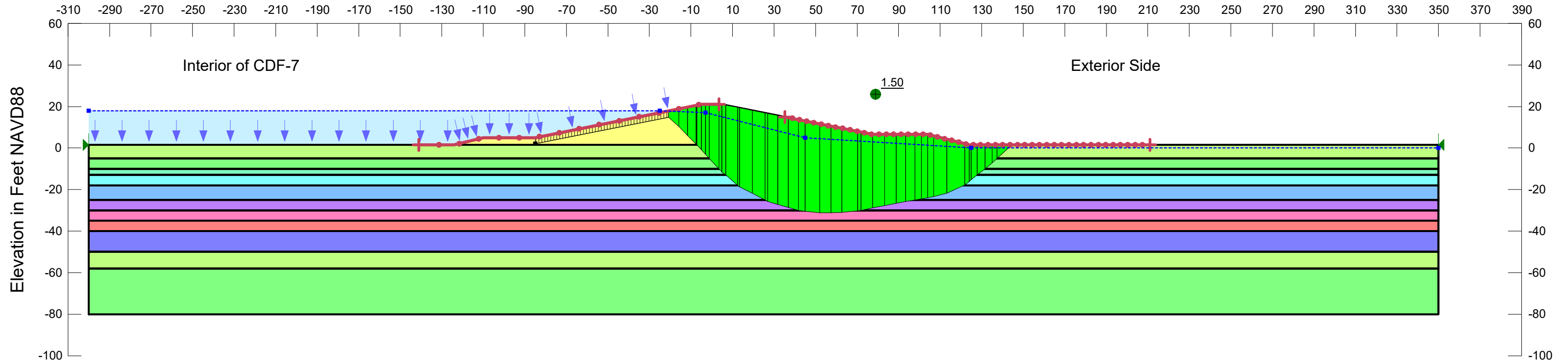
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Low Water Level - Entry Exit Slip Surface
 Louisiana

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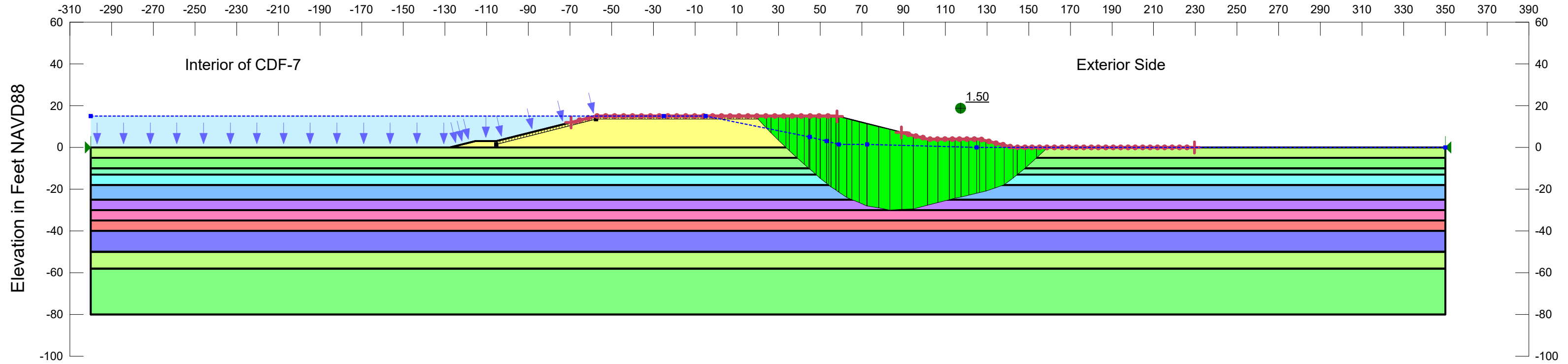
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**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Still Water Level - Entry Exit Slip Surface
 Louisiana



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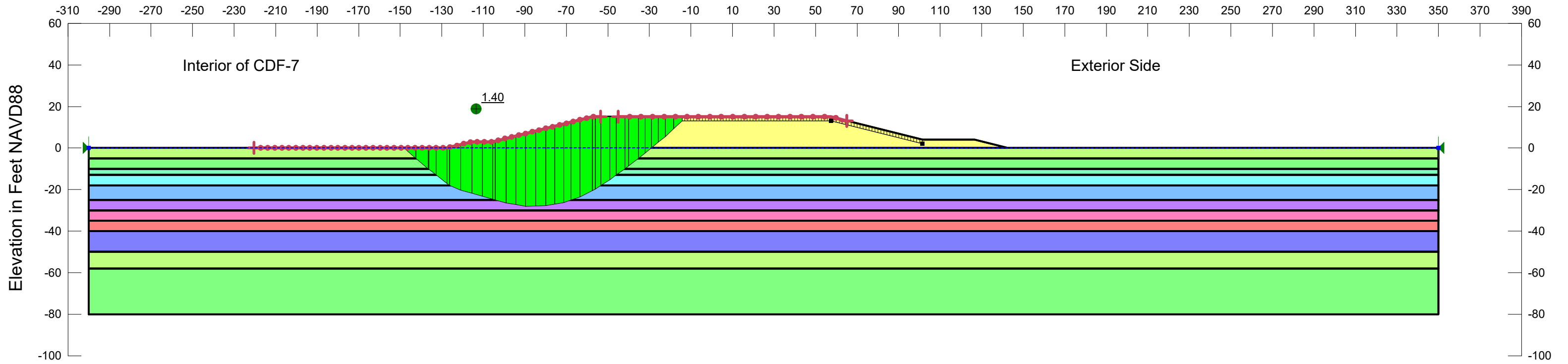
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Top of Levee - Entry Exit Slip Surface
 Louisiana

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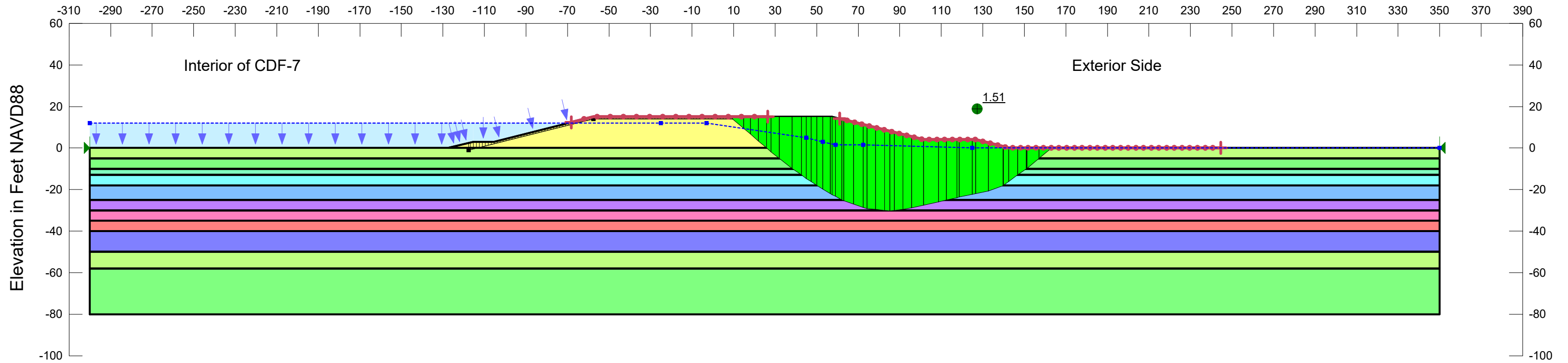
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Low Water Level - Entry Exit Slip Surface
 Louisiana

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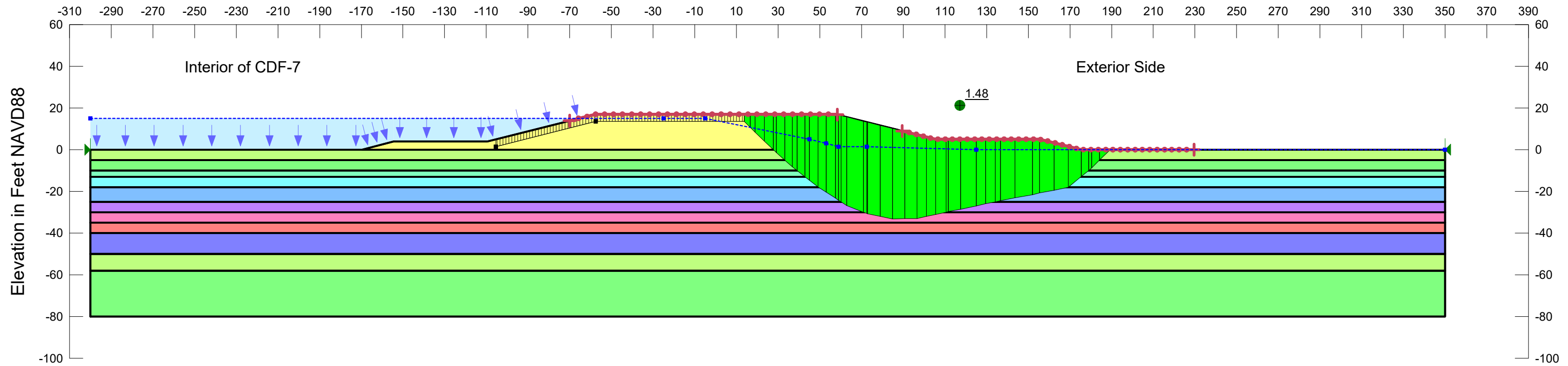
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 6

Still Water Level - Entry Exit Slip Surface
 Louisiana

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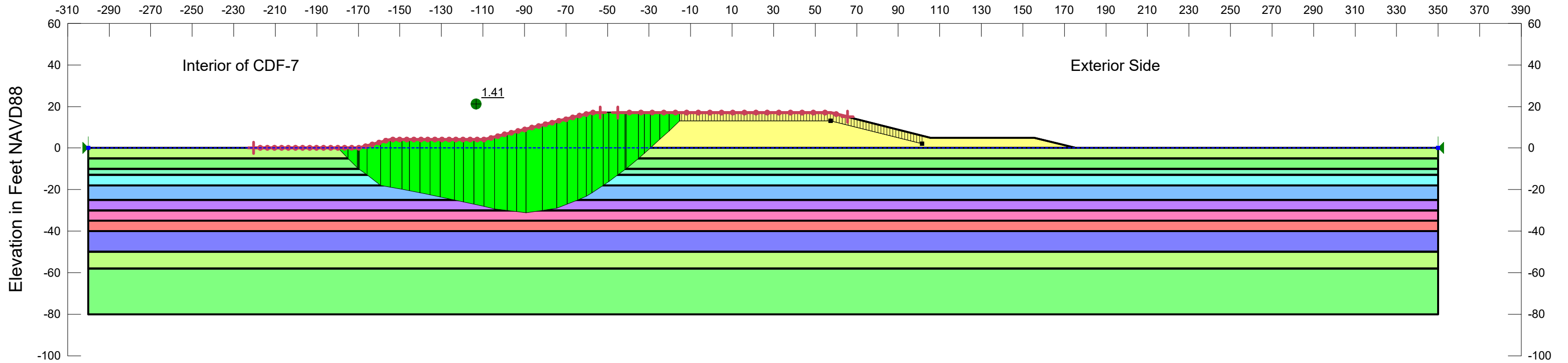
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 8

Top of Levee - Entry Exit Slip Surface
 Louisiana

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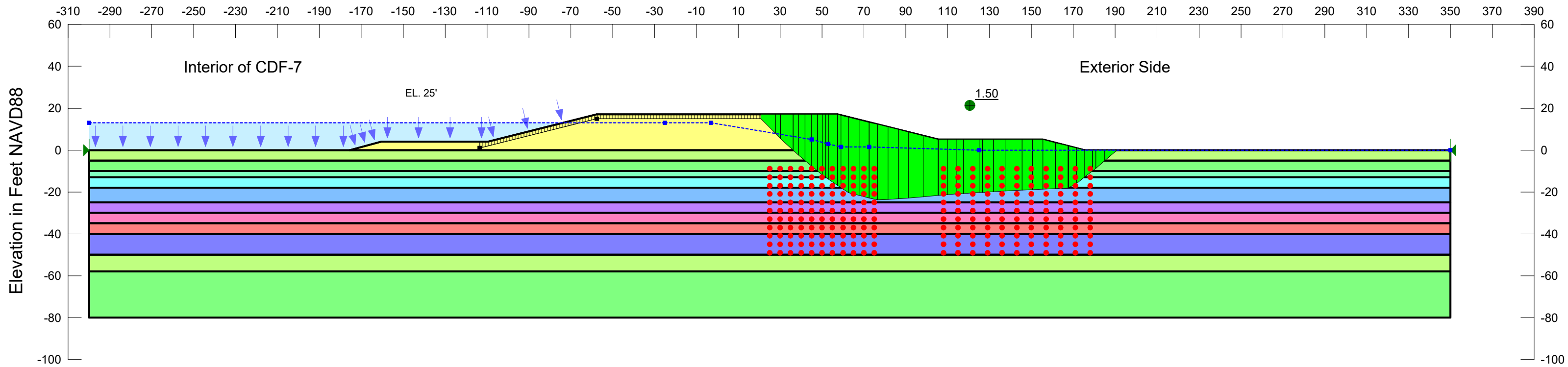
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**US Army Corps
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 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 8

Low Water Level - Entry Exit Slip Surface
 Louisiana

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Gains in Strength from additional loadings were added for this stability analysis

GENERAL NOTES

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 SHEAR STRENGTHS AND UNIT WEIGHTS OF
 THE SOIL WERE BASED ON THE RESULTS OF
 UNDISTURBED BORINGS. SEE
 BORING DATA PLATES.

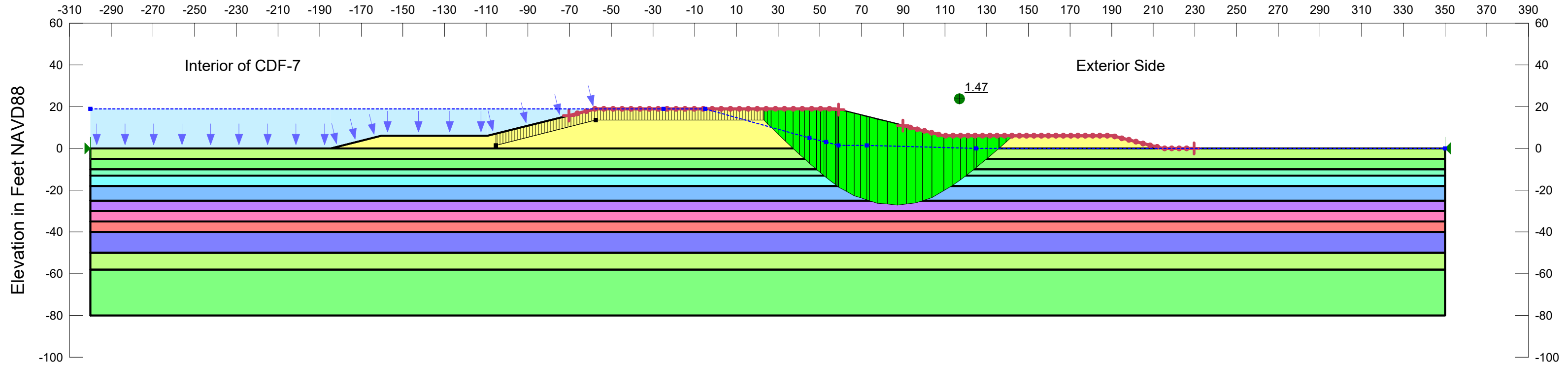
SHEAR STRENGTHS BETWEEN VERTICALS
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 THE VALUES INDICATED FOR THESE LOCATIONS.



**US Army Corps
 of Engineers**
 New Orleans District
 Upper Barataria Basin
 Stability Analysis for Cost Estimate
 Alternative 8

Still Water Level - Block Slip Surface
 Louisiana

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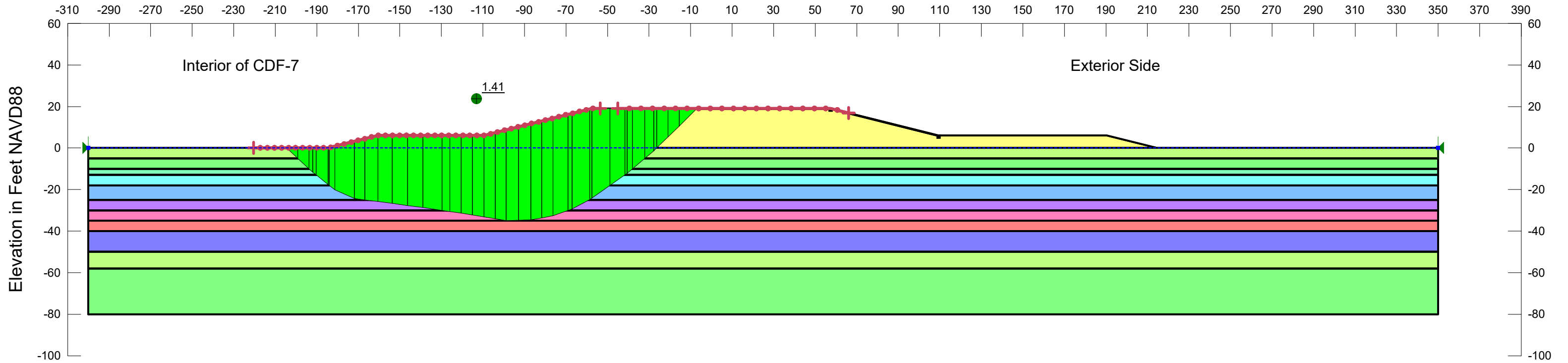
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Top of Levee - Entry Exit Slip Surface
 Louisiana

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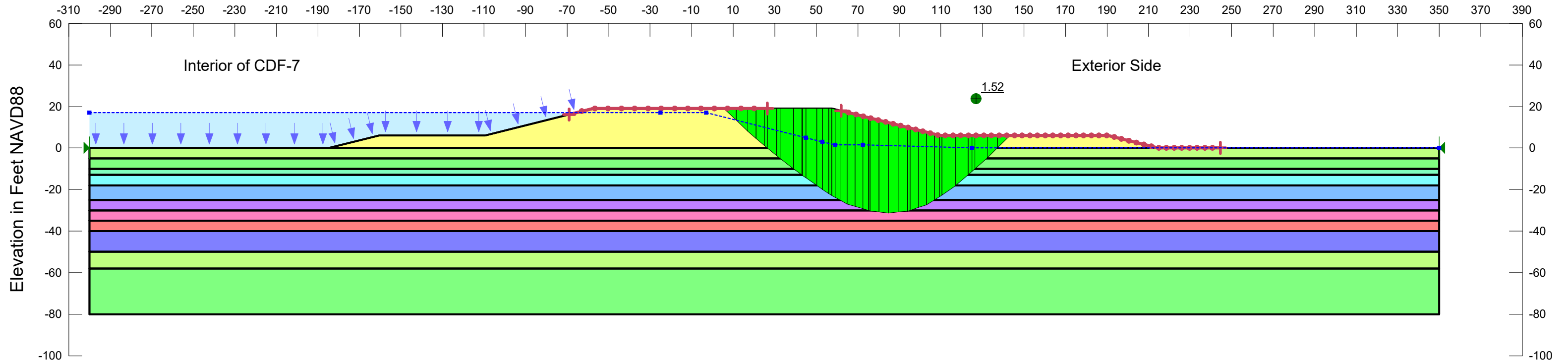
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 New Orleans District
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Low Water Level - Entry Exit Slip Surface
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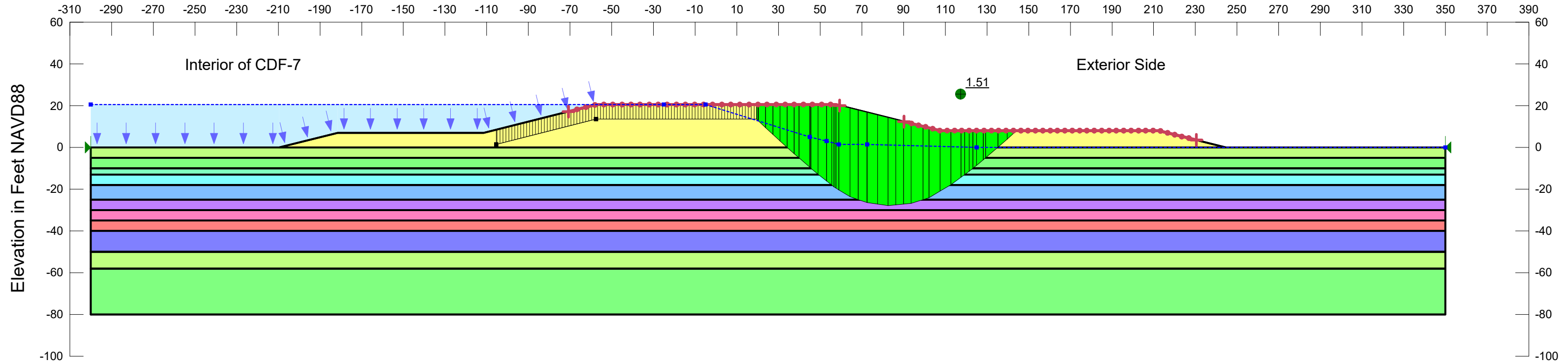
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 New Orleans District
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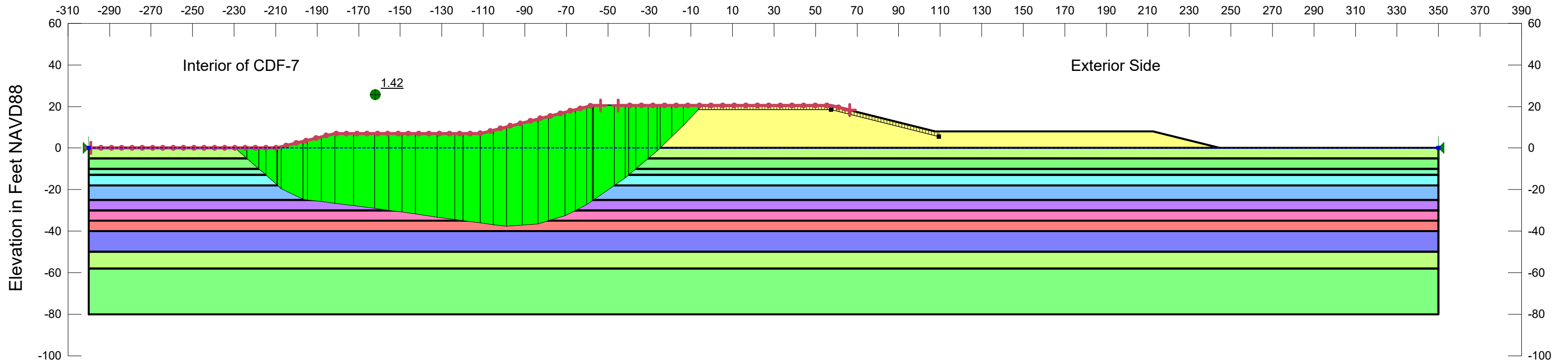
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 New Orleans District
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Top of Levee - Entry Exit Slip Surface
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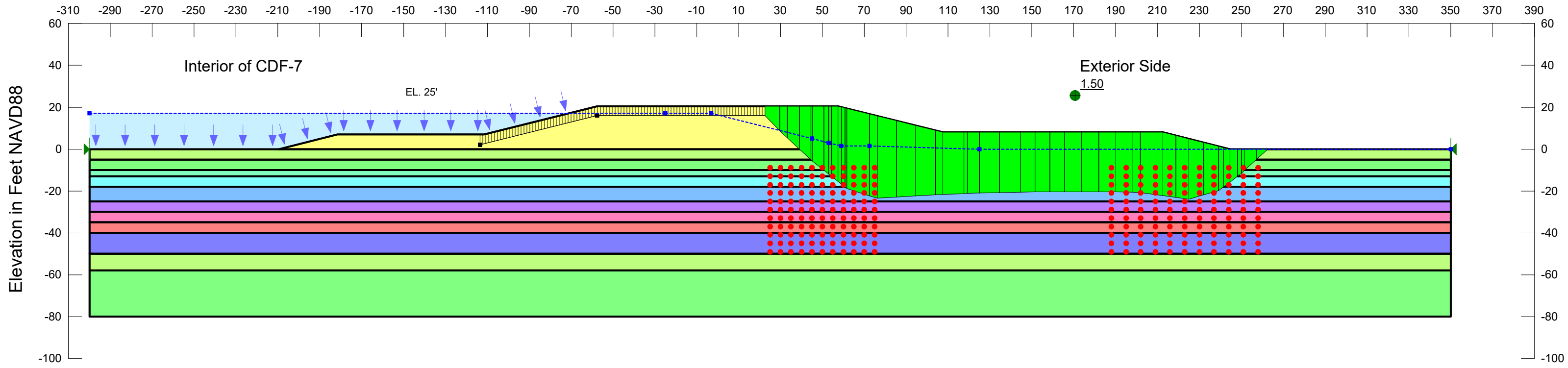
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